

Harnessing disorder for photonic device applications



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ABSTRACT

For photonic devices, structural disorder and light scattering have long been considered annoying and detrimental features that were best avoided or minimized. This review shows that disorder and complexity can be harnessed for photonic device applications. Compared to ordered systems, disordered systems provide much more possibilities and diverse optical responses. They have been used to create physical unclonable functions for secret key generation, and more recently for random projection, high-dimensional matrix multiplication, and reservoir computing. Incorporating structural disorder enables novel devices with unique functionalities as well as multi-functionality. A random system can function as an optical lens, a spectrometer, a polarimeter, and a radio frequency receiver. It is also employed for optical pulse measurement and full-field recovery. Multi-functional disordered photonic devices have been developed for hyperspectral imaging, spatial, and spectral polarimetry. In addition to passive devices, structural disorder has been incorporated to active devices. One prominent example is the random laser, which enables speckle-free imaging, super-resolution spectroscopy, broad tunability of high-power fiber laser, and suppression of lasing instabilities. Disordered devices have low fabrication costs, and their combination with advanced computational techniques may lead to a paradigm shift in photonics and optical engineering.

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I. INTRODUCTION

While most photonic devices are designed to have regular, ordered structures, disordered structures provide much more possibilities. Compared to a periodic array of particles with identical size and shape [Fig. 1(a)], disorder may be introduced to spatial position, size, and shape of an individual particle [Fig. 1(b)]. An ordered structure has only a few spatial frequencies [Fig. 1(c)], but a disordered structure contains many more spatial frequencies [Fig. 1(d)], providing a huge parameter space for device design. Consequently, an inverse design of photonic devices, namely, optimizing device configurations for desired functionalities, often ends up with “seemingly” disordered structures instead of ordered ones.¹

Over the years, there have been growing interest and efforts in harnessing disorder for photonic device applications. More and more examples show that incorporating disorder not only improves the performance of existing devices, but also enables novel schemes and additional functionalities. Disordered structures are easy to fabricate and have low costs, while providing diverse responses to external signals. As photonic devices, their functionalities often rely on post-processing of their responses using computational algorithms, including compressive sensing and machine learning. Such algorithms have advanced rapidly in recent years; meanwhile, physical size and cost of processors have fallen sharply. Therefore, the emergence of disordered photonic devices enables a paradigm shift of device design from hardware to software, which will dramatically lower the cost.

A. Motivation

In this subsection, we will present a few examples to illustrate some of the advantages for incorporating disorder to photonic devices. More details and relevant references can be found in Secs. IA 1–IA 4.

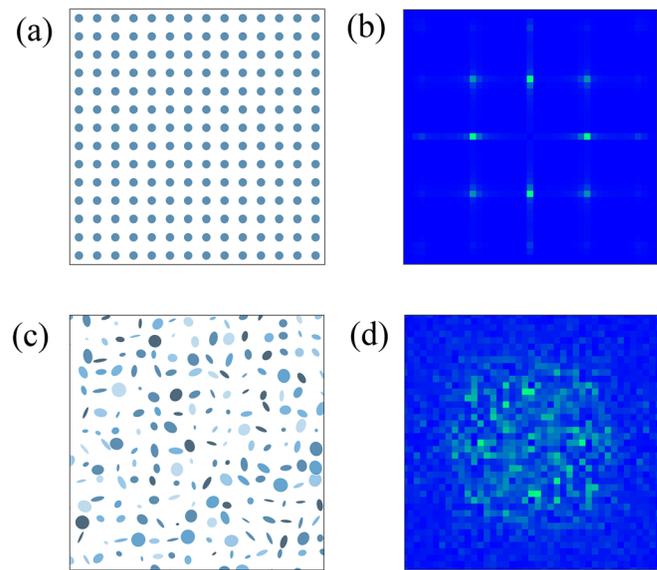


FIG. 1. Order vs disorder. A periodic array of particles with identical size and shape in (a) has only a few well-defined spatial frequencies (b). A disordered array of particles with irregular size and shape and varying refractive index in (c) contains many spatial frequencies (d).

1. Optical physical unclonable functions (PUFs) for secret key generation

A disordered system packed with billions of micro- or nanoparticles possesses an enormous amount of entropy, and features diverse optical responses to external interrogations.² As illustrated in Fig. 2, directing a laser beam to a bulk random sample will generate a seemingly random grainy pattern (speckle) in transmission or reflection (response), which depends on the illumination condition (challenge). The huge number of challenge–response pairs makes a complete characterization impossible, and machine learning attacks ineffective. Moreover, it is extremely difficult, if not impossible, to clone the random dense packing of numerous particles with irregular size and shape to reproduce the response (speckle pattern). The extraordinary complexity, uniqueness, high sensitivity, and low fabrication costs make the random scattering media an ideal candidate of strong PUFs for authentication and information security.

2. Random spectrometers

Most spectrometers use periodic gratings to diffract light of different wavelengths to different directions, so that they are spatially separated and measured by different sensors. Figure 3(a) shows one-to-one spectral-to-spatial mapping; that is, each wavelength is mapped to a single spatial location. If the location falls outside a sensor array, the corresponding wavelength will not be detected at all. To cover different spectral range, the grating must be rotated. Such rotation is extremely challenging, if not impossible, to implement with a monolithic grating in an on-chip spectrometer.

If the periodic grating is replaced by a disordered structure, random diffraction will project a signal to all sensors, regardless of its wavelength. Every wavelength generates a distinct spatial distribution

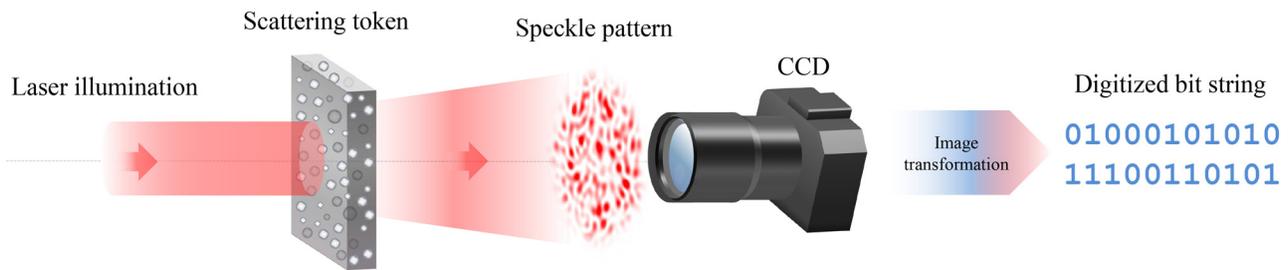


FIG. 2. Physical unclonable function (PUF) for secure key generation. A coherent laser beam impinges on a 3D linear scattering medium (token) and generates a random speckle pattern as response. The pattern is recorded by a 2D camera and digitally processed to extract a bit string as the key. An enormous number of keys can be generated by varying the spatial position and incident angle of the illumination beam to create different speckle patterns.

of light intensity across the sensor array and can be used as “fingerprint” for spectral reconstruction.³ As shown in Fig. 3(b), the one-to-many spectral-to-spatial mapping allows a small number of sensors to cover a broad wavelength range, even with a fixed disordered structure. The spectrum cannot be directly readout from the sensor array; instead, it will be reconstructed by computational algorithms. Compressive sensing techniques have been developed to increase the number of spectral channels that can be recovered from a single acquisition.

For grating/prism or resonant-cavity-based spectrometers, the free spectral range (FSR) sets an upper bound of wavelength range in one measurement. In sharp contrast, the random spectrometer does not have the FSR limit, because a disordered structure lifts all degeneracies. The probability of having identical output patterns at well-separated wavelengths is negligible. Furthermore, multiple scattering

of light provides non-resonant broadband enhancement of wavelength resolution, enabling a chip-scale spectrometer with small footprint and fine resolution.

3. Multi-functional photonic devices

Complex optical systems, for example, disordered photonic nanostructures, multimode fibers with random refractive index fluctuations, have numerous degrees of freedom (DoFs) in space, time, spectrum, and polarization. Since these DoFs are coupled, it is possible to use the DoFs in one domain at input to control the output in another domain. For example, the transmission spectrum,^{4,5} polarization state,^{6–8} and temporal pulse shape^{9–16} can be varied by shaping the spatial wavefront of incident light.¹⁷ Hence, a complex system, in combination with a spatial light modulator (SLM), can function simultaneously as a temporal pulse shaper, a reconfigurable waveplate, a tunable spectral filter, and a programmable beam splitter.¹⁸

Inversely, a complex optical system allows recovery of information of an input signal in one domain by measuring the output light in a different domain. As an example, the spatial intensity distribution (speckle pattern) of transmitted light through a disordered medium or a multimode fiber encodes the information of spatial wavefront, spectrum, and polarization state of the incident wave. Such information of input may be retrieved from the output speckle measurement, meaning a single system can serve as a lens, a spectrometer, and a polarimeter. It is also possible to simultaneously recover information in multiple domains, for example, reconstructing both spatial and spectral distributions of a signal from one speckle pattern, enabling snapshot hyperspectral imaging.

4. Suppression of coherent imaging artifacts

Spatial coherence of laser emission introduces coherent artifacts like speckle noise, limiting the use of lasers as illumination sources in full-field imaging applications including wide-field microscopy, parallel projection, optical holography, and photolithography. A common method of reducing the spatial coherence of a laser is integrating many different speckle patterns generated by a time-varying scattering system like a rotating or vibrating diffuser [Fig. 4(a)]. Such scheme is slow and inefficient, as it starts with a coherent laser and then reduces the coherence with a diffuser outside the laser. A more direct and efficient approach is to design a laser with low spatial coherence by inserting a diffuser into the cavity, or more generally, by incorporating

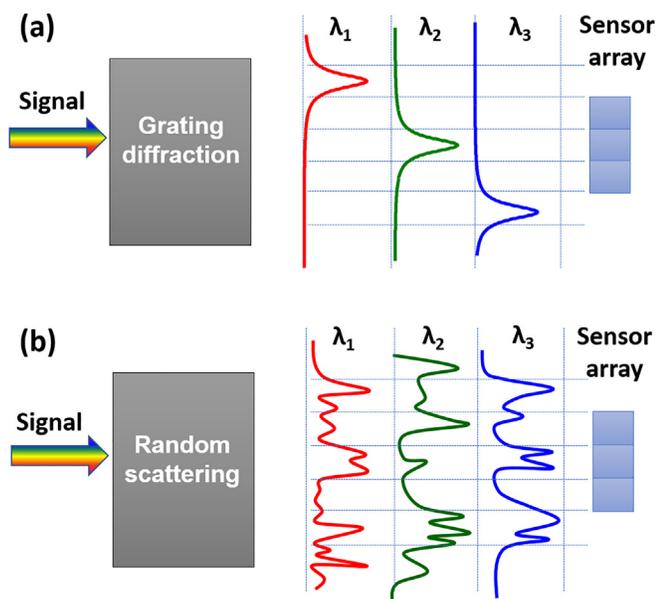


FIG. 3. Conventional spectrometer vs random spectrometer. (a) A grating spectrometer maps individual wavelengths to different spatial positions. The wavelengths that miss the sensor array will not be detected at all. (b) A disordered structure generates a random scattering pattern unique for each wavelength, and no wavelength will miss the sensor array.

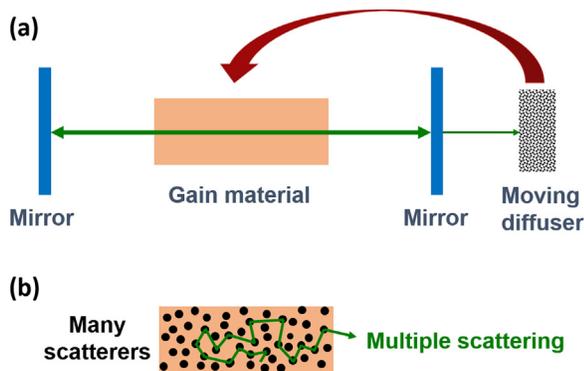


FIG. 4. Conventional laser vs random laser. A standard laser consisting of a gain material in between two mirrors produces spatially coherent emission. To avoid coherent imaging artifacts with laser illumination, the spatial coherence of laser emission is lowered by placing a moving diffuser outside the cavity (a) or incorporate many scatterers inside the gain material (b). Light amplification is enhanced by multiple scattering that increases optical path length inside the gain material.

scatterers to a gain material [Fig. 4(b)]. Such a laser is called a random laser, and it can produce emission with varying degrees of spatial coherence. Its brightness as a laser enables high-speed full-field imaging, and its relatively low spatial coherence rejects speckle and coherent crosstalk.

B. Background

In this subsection, we will define relevant parameters and functions, and introduce physical phenomena and mechanisms that underlie the photonic devices in Secs. IB 1–IB 6.

1. Photonic systems with disorder

In this review, we consider mostly disordered photonic structures of varying parameters and dimensions. Examples are one-dimensional (1D) dielectric layers with fluctuating thickness/refractive index, two-dimensional (2D) arrays of cylindrical holes randomly distributed in a membrane, and three-dimensional (3D) packing of nanoparticles with irregular size and shape. In addition, we will include optical cavities featuring chaotic ray dynamics such as integrating spheres with rough inner walls, and optical fibers with structural inhomogeneities and refractive index variations.

2. Characteristic lengths of optical scattering

Light is scattered by a disordered structure with refractive index variation on the length scale of the optical wavelength. The scattering strength is characterized by the scattering mean free path l_s and the transport mean free path l_t . The scattering mean free path l_s is defined as the average distance that light travels between two consecutive scattering events. The transport mean free path l_t is defined as the minimum distance a wave travels before its direction of propagation is completely randomized. These two length scales are related by

$$l_t = \frac{l_s}{1 - \langle \cos \theta_s \rangle}, \quad (1)$$

where $\langle \cos \theta_s \rangle$ is the average cosine of the scattering angle θ_s , which can be found from the differential scattering cross section. If the scattering particle size is smaller than the wavelength λ , Rayleigh scattering of light gives $\langle \cos \theta_s \rangle = 0$, and $l_t = l_s$. For larger scatterers, Mie scattering results in $\langle \cos \theta_s \rangle \approx 0.5$, and $l_t \approx 2l_s$.

3. Light diffusion and localization

In a scattering system of thickness L_s that is less than l_s , light is scattered only once. When L_s exceeds l_s , light is scattered multiple times. Once $L_s \gg l_t$, light transport can be described by diffusion. The total transmission (transmittance) is on the order of $l_t/L_s \ll 1$. Random walk of photons increases their path-lengths inside the scattering system. The average path length for transmitted light is $\langle \mathcal{L} \rangle \sim L_s^2/l_t$. Multiple scattering and light diffusion leads to a broad distribution of optical path-lengths \mathcal{L} , and its width $\Delta \mathcal{L}$ is comparable to the mean path length.

In 1D and 2D disordered systems, light will be localized, as long as the system size is sufficiently large (exceeding the localization length). It is hard to localize light in 3D disordered systems, even in the presence of strong scattering. Unlike the linear decay in the diffusive regime, the average transmission of light in the localization regime decays exponentially with the system thickness L_s . Almost all light will be reflected back, when absorption is negligible.

4. Multimode optical fiber

In a multimode fiber (MMF), intrinsic imperfections like refractive index variation along the fiber and external perturbations that cause fiber bending or twisting result in optical coupling between guided modes. Such coupling can be considered as optical scattering in the fiber modal space. The effective scattering mean free length l_s is given by the average distance light travels in the fiber before hopping from one spatial mode to another. The effective transport mean free path l_t is the minimum propagation distance beyond which light is spread over all fiber modes, no matter which mode is initially launched into. If the fiber length L_{MMF} is shorter than l_t , then the mode coupling is weak. Once $L_{\text{MMF}} \gg l_t$, the mode coupling is strong enough to initiate a random walk of photons in the modal space. Since backscattering is negligible, light diffusion occurs in the modal space, namely, light always propagates forward in the fiber, but in different spatial modes.

The modal dispersion (group velocity dispersion) in a MMF broadens the path length distribution of transmitted light. If the mode coupling is weak, the width of optical path length distribution scales linearly with the fiber length, $\Delta \mathcal{L} \propto L_{\text{MMF}}$. In the strong coupling regime, light is scattered back and forth among the fiber modes, and the optical path length distribution is narrowed. Its width scales as $\Delta \mathcal{L} \propto \sqrt{L_{\text{MMF}}}$, as a result of diffusion.

5. Spectral correlation function

The speckle field pattern $E_p(r, \lambda)$, generated by coherent light transmitted through a random scattering medium, varies with wavelength λ . The spectral field correlation function is defined as

$$C_E(\Delta\lambda) \equiv \frac{\langle E_p^*(r; \lambda) E_p(r; \lambda + \Delta\lambda) \rangle_{r, \lambda}}{\langle |E_p(r; \lambda)|^2 \rangle_{r, \lambda}} - 1, \quad (2)$$

where $\langle \dots \rangle_{r, \lambda}$ represents averaging over spatial position r and wavelength λ . The spectral correlation function for speckle intensity, $C_I(\Delta\lambda)$, is equal to $|C_E(\Delta\lambda)|^2$, if non-local correlation is negligible. The full-width-at-half-maximum (FWHM) of $C_I(\Delta\lambda)$ is inversely proportional to the width of optical path length distribution $\Delta\mathcal{L}$. In a diffusive system without absorption, the spectral correlation width scales as l_t/L_s^2 .

Similarly, $\Delta\mathcal{L}$ in a MMF determines how fast the transmitted speckle pattern decorrelates with wavelength. In a fiber with weak mode coupling, the spectral correlation width scales as $1/L_{\text{MMF}}$. With strong mode coupling, the scaling is changed to $1/\sqrt{L_{\text{MMF}}}$.

If the input light has a bandwidth narrower than the spectral correlation width, it can be considered as “monochromatic” in terms of transport through a scattering medium or a MMF. The transmitted speckle, if fully developed, has an intensity contrast $C_t \equiv \sigma_I/\bar{I}_s = 1$, where σ_I is the standard deviation of intensity, \bar{I}_s is the mean intensity. For a broadband input whose bandwidth is N_λ times of the spectral correlation width, the transmitted intensity pattern is an incoherent sum of N_λ distinct speckle patterns, and the speckle intensity contrast C_t is reduced to $1/\sqrt{N_\lambda}$.

6. Optical memory effect

The angular memory effect in random scattering systems, also referred to as intrinsic isoplanatism, is a key physical phenomenon that has been widely used for optical imaging, metrology, and communication through turbid media. When the spatial wavefront of a coherent beam incident on a disordered slab is tilted by a small angle, the transmitted wavefront is tilted by the same angle, leading to a lateral translation of the far-field speckle pattern. The angular memory effect exists in both single-scattering and multiple-scattering systems. The angular range of memory effect is inversely proportional to the system thickness, and thus, a thin diffuser has a large memory effect range.

Consider a diffusive slab of width much larger than its thickness L_s , a point excitation at the front surface of the slab emerges as a diffusive halo of radius $\sim L_s$ at the back surface. This lateral spread determines the angular range of memory effect, $\Delta\theta_m = \lambda/(2\pi L_s)$. The angular memory effect also exists for light reflected from the slab. Since the penetration depth is on the order of transport mean free path l_b , the angular range of memory effect in reflection is approximately $\lambda/(2\pi l_t)$.

C. Scope

This review aims to illustrate why structural disorder is useful for photonic device applications, and how it has been incorporated to both passive and active devices. Here, we focus on the methods and mechanisms of utilizing “randomness” (natural disorder) to enhance device performance and add new functionality, without relying on “controlled” disorder. Even when structural disorder is intentionally introduced to a device, the exact configuration is not necessarily known. The disorder is neither correlated nor engineered.

In this review, we start with passive devices (Secs. II–VII) and then move to active ones (Sec. VIII). One category of disordered photonic device applications is information security and optical

computing. Section II describes the construction of optical physical unclonable functions with random complex systems for secure key generation. The emerging applications of disorder for optical computing and artificial neural network are discussed in the last section (Sec. IX).

Another category of disordered device applications is imaging and sensing. In Secs. III–VII, random systems are employed to retrieve spatial, spectral, temporal, and polarization information of light fields, so that they function as optical lens (Sec. III), spectrometer or wave-meter (Sec. IV), polarimeter (Sec. VI), and RF receiver (Sec. VII A), and are also used for optical pulse measurement and full-field recovery (Sec. VII B). Multi-functional devices are developed for hyperspectral imaging (Sec. V), and spatial and spectral polarimetry (Sec. VI). These applications require the random systems to have static structures and constant environments. If the illuminating light is fixed, the optical response of a random system can be used to monitor environmental change, and disorder-induced light scattering will enhance the sensitivity, as shown in Sec. IX A.

Shifting from passive devices to active devices, we will introduce random lasers and their applications for speckle-free imaging and super-resolution spectroscopy in Sec. VIII. This section also presents remarkable performance that random fiber lasers have achieved in terms of high-power generation and ultra-broad frequency tunability, as well as the unexpected suppression of lasing instabilities by disorder.

Figure 5 presents a roadmap of this review. In Table I, the disordered photonic devices covered in this review are summarized.

The scope of this review is restricted to *intentional* use of disorder for photonic *device* applications. To provide a tutorial for newcomers, our review of existing works does not follow the chronological order. For related topics that are not covered here, there are excellent reviews and books regarding fundamental physics of light scattering and wave transport in disordered systems,^{19–25} control of light transport by wavefront shaping,^{17,26,27} mitigating the effects of naturally occurring disorder and optical scattering for imaging and sensing applications,^{28–31} disordered photonics and optics^{32,33} in general, and correlated and engineered disorder^{34–36} in specific.

II. PHOTONIC PHYSICAL UNCLONABLE FUNCTIONS

In this section, we introduce different types of optical physical unclonable functions (PUFs) that have been developed with random, chaotic systems for physical key generation. After a brief introduction of PUFs in Sec. II A, we describe the strong optical PUFs based on linear light scattering (Sec. II B) and show how the PUFs can be made reconfigurable (Sec. II C). To enhance security, nonlinear PUFs (Sec. II D) and quantum readouts (Sec. II E) are developed. Finally, we discuss strong photonic PUFs (Sec. II F) and weak ones (Sec. II G).

A. Introduction of PUFs

The physical unclonable function (PUF), originally named physical one-way function, is the modern realization of a physical key. It represents an unpredictable yet deterministic physical system that creates a reproducible output for a given input. The input-to-output mapping is unique for every token and is characterized by implementing a challenge-response protocol. The PUF is interrogated with a list of input signals called challenges, and the output signals, called responses, are recorded and processed. An applied challenge and the measured

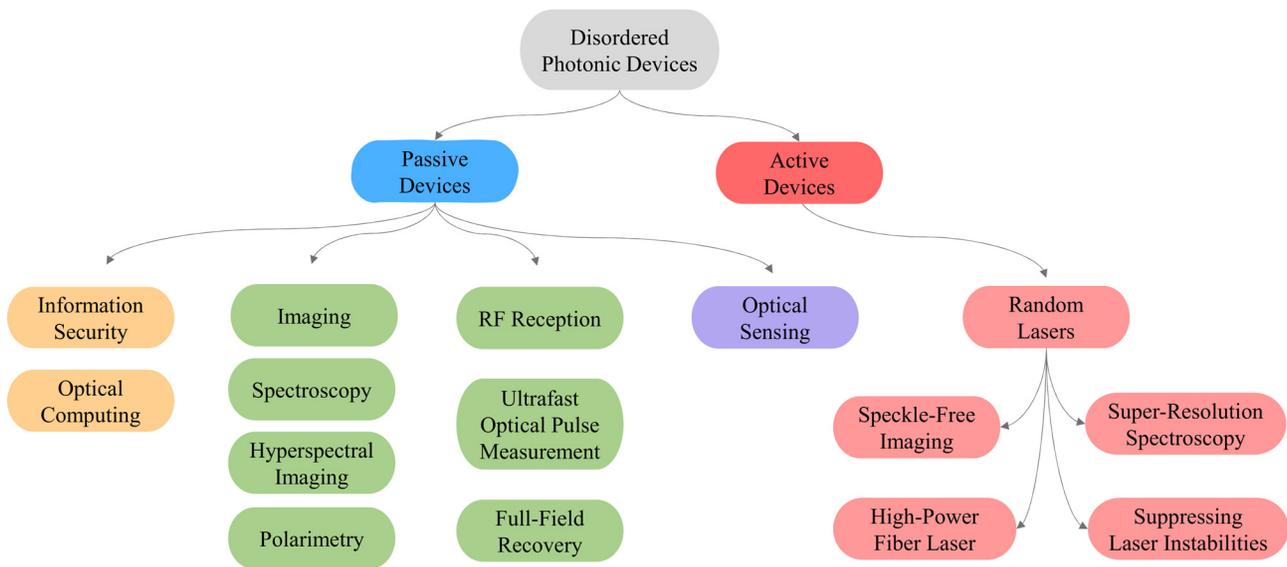


FIG. 5. Roadmap of this review. The review covers both passive and active disordered devices for various photonic applications. The passive devices are grouped according to information security and computing, imaging and metrology and sensing applications. The active devices are a group of disordered lasing applications.

response are referred to as a challenge–response pair (CRP). During the enrollment phase, a challenge–response library is created. Based on the maximum size of the library, PUFs are classified as weak PUFs or strong PUFs. Strong PUFs differ from their weak counterparts by an extremely large CRP space, which is fully accessible to any user or attacker and impossible to entirely readout in feasible time. The challenge–response mapping is so complex that the response to a fresh challenge is hard to predict.

In general, PUFs exploit the unique and inherent randomness of physical micro-structures originating from fabrication and environmental conditions for authentication and information security.^{37,38} Optical PUFs, in particular, utilize various optical processes in disordered structures for interrogation and readout.³⁹ This section reviews the developments of photonic PUFs, with a focus on strong PUFs.

B. Linear scattering PUFs

The first optical PUF is realized with a three-dimensional (3D) bulk of randomly packed glass spheres² serving as a token (Fig. 2). When a laser beam is incident to the token, light experiences multiple scattering. The interference of scattered waves generates a random grainy intensity profile—a speckle pattern.⁴⁰ With static scatterers, the optical scattering is a deterministic linear process. The resulting speckle pattern is reproducible for a fixed scatterer’s configuration and a given illumination condition. The PUF challenge is set by the illumination conditions such as wavelength, spatial location, and incident angle of the laser beam. The PUF response is a digitized bit string extracted from the speckle pattern of transmitted/reflected light.

Such an optical PUF has a very large number of possible challenges.^{2,41} Consider a scattering slab with a cross section area of 1 cm^2 and thickness of 2.5 mm . A monochromatic light at the wavelength of 500 nm can be coupled into any one of the 10^9 spatial modes at the input facet to produce a distinct output speckle pattern. This enormous

space renders the complete readout of all challenge–response pairs (CRPs) an extremely challenging task, even if an adversary holds physical possession of the PUF for a considerable time.

While it is easy to fabricate a 3D scattering PUF, it is impossible to clone one with the state-of-the-art technology. A 0.25-cm^3 token consists of 10^{11} scattering particles of average diameter $\sim 1\ \mu\text{m}$. These particles are randomly packed in a 3D volume and have polydisperse size and irregular shape. It is extremely difficult to accurately determine their position, size, and shape, let alone duplicate them with high precision. Even with the exact knowledge of the entire 3D structure, it is impossible to numerically calculate the response to a given challenge in a reasonable time. Since the speckle pattern is very sensitive to any modification of the scattering structure, the PUF is intrinsically tamper-resistant.^{2,41,42}

To this day, the optical scattering PUF has withstood any machine learning-based modeling attacks,⁴¹ while most existing electronic PUF architectures have failed.³⁹ In such attacks, machine learning (ML) algorithms are trained with a subset of the CRP space to extrapolate and predict the entire space. The resistance of optical scattering PUFs to ML attack attempts is achieved by interrogating different spatial regions of a random bulk material. The interrogation of different spatial regions where the scattering structure is entirely different yields new speckle patterns, uncorrelated to the previous patterns that the algorithm has already learned.

Therefore, the extraordinary complexity of random-scattering optical PUF provides an unprecedented security level; however, it comes at the cost of a large device size and lack of electronic integration. Moreover, the response repeatability or reliability requires a sub-micrometer precision in positioning the token with respect to the interrogating beam and the camera, which is difficult to implement in a cost-effective way.

To overcome these issues, miniaturization and integration of optical scattering PUFs to electronic circuits have been explored.^{41,43,44}

TABLE I. Detailed summary of the disordered photonic devices covered in this review.

Device	Functions	Disorder-enabled features	Type	Sections
Physical unclonable function (PUF)	Secret key generation	Extraordinary complexity, reconfigurability, high security, robustness against attacks	Passive	II
Optical computing	Random projection, reservoir computing	High dimensionality, scalability, reconfigurability	Passive	IX B
Random lens	Spatial imaging, light focusing	Enhanced spatial resolution, enlarged field-of-view	Passive	III
Speckle spectrometer, wavemeter	Spectrum reconstruction, wavelength identification	Overcoming the trade-off between device size and spectral resolution, elimination of free-spectral range	Passive	IV
Hyperspectral imager	Spectrally resolved imaging	Single acquisition, flexible adjustment of spatial-spectral trade-off, insensitivity to optical (mis)alignment	Passive	V
Scattering polarimeter	Spatially and/or spectrally resolved polarimetry	Retrieval of spatial, spectral and polarization information with a single speckle pattern	Passive	VI
Compressive RF receiver	Radio-frequency reception	Breaking Nyquist sampling limit with compressive sensing technique	Passive	VII A
Optical pulse measurement	Pulse shape recovery, full-field measurement	Time-integrated measurement, reference-free, removal of ambiguity in the direction of time	Passive	VII B
Optical sensor	Monitoring of temperature, pressure, mechanical motion, refractive index variations	High sensitivity, multi-functional sensor, simple implementation	Passive, active	IX A
Random laser illumination source	Speckle-free full-field imaging	High spectral radiance, low spatial coherence, fast decoherence, short integration time	Active	VIII B and VIII C
Super-resolution spectroscopy	Sparse spectral sampling with random lasing peaks	Breaking the spectrometer resolution limits	Active	VIII D
Fiber random laser	High power generation	High efficiency, clean output beam, nearly octave wavelength tuning	Active	VIII E
Disordered semiconductor laser	Stable lasing dynamics	Suppression of temporal instability over a wide range of pump power	Active	VIII F

In one proposal, the PUF challenge space is comprised of illumination patterns generated by an integrated spatial light modulator or an array of phase-locked laser diodes. However, integrable optical PUFs are vulnerable to modeling and ML attacks, because of the reuse of a compact scattering volume and the linear nature of the optical scattering process.⁴¹ Once the linear relation between the input field and the output field is characterized or learned, the response to any challenge can be predicted.

C. Reconfigurable optical PUFs

One way to avoid the reuse of a scattering structure is to reconfigure the scattering structure and increase the structural diversity. This is done by heating a polymer containing randomly distributed scattering particles with an intense laser beam.⁴⁵ Once the polymer melts locally, the scattering particles change their position and subsequently freeze after cooling down. Alternatively, a polymer-dispersed liquid crystal film is reconfigured with the application of an electrical voltage

in a short amount of time.⁴⁶ The reconfigured scattering potential is uncorrelated with respect to its prior, effectively erasing the old PUF and creating a new one. This property of total erasability allows a complete destruction of the old PUF and prevents the abuse of a security device that falls into adversarial hands. While both reconfiguration schemes generate new unpredictable structures, they cannot return to the old ones. Such irreversible reconfigurability allows a single PUF-carrying hardware to be refreshed and employed by different customers sequentially. However, in between the reconfiguration operations, the input-output mapping remains linear, making the PUF vulnerable to ML attacks.

D. Nonlinear optical PUFs

Given the vulnerabilities of linear optical PUFs, optical nonlinearities in a silicon chip are harnessed for the construction of an integrated PUF.^{47,48} The nonlinear optical PUF exploits ultrafast nonlinear light-matter interactions in a two-dimensional (2D)

microcavity.⁴⁷ The cavity shape is designed to induce chaotic ray dynamics, and air holes are arbitrarily positioned within the silicon cavity to cause light scattering (Fig. 6). Despite the state-of-the-art fabrication techniques, the microcavities possess inevitable structural and compositional idiosyncrasies that cannot be duplicated. The PUF challenges are encoded in the spectrum modulations of femtosecond laser pulses. Once the pulses are injected into a silicon microcavity, their high intensities trigger nonlinear optical processes including Kerr effects and free-carrier absorption. The output pulses are spectrally filtered and digitized to provide the PUF responses. The nonlinear input–output relation makes the PUF robust against ML attacks.⁴⁸

E. Quantum readout

The aforementioned PUFs use classical light for readout, and thus, they are vulnerable to emulation attacks.³⁷ Despite an enormous number of possible CRPs, only a small portion can be characterized and stored in a database. Once an adversary gains access to the challenge–response database, it is possible to intercept the challenges and produce the correct responses, if the interrogation is conducted with classical light. To defend against the digital emulation, quantum readout of PUFs is introduced.⁴⁹ The challenges are high-spatial-dimension states of light with only a few photons. When the number of spatial modes exceeds the number of photons, it is impossible for an adversary to fully determine the challenge and therefore to construct the expected response.⁵⁰ This scheme no longer depends on the secrecy of any stored data.

F. Strong PUFs

Strong PUFs have been realized in various optical systems, with no means of cloning. In addition to disordered photonic nanostructures, random coupling of spatial modes in an optical fiber/waveguide is explored for PUF construction^{51,52} and classical⁵³ or quantum⁵⁴ key establishment. Beyond the spatial domain, spectral features created by

disorder in an optical waveguide are exploited for an integrated photonic PUF.⁵⁵ More recently, a disordered metasurface embedded with perovskite quantum dots provides fluorescent speckle patterns with enormous encoding capability.⁵⁶ While it has been mostly used to attack PUFs, deep learning is employed in optical PUF generation to improve reliability and unpredictability.⁵⁷

Since the photonic PUFs are unique, unpredictable, reproducible (only by themselves), unclonable (even by manufacturers), one-way (non-invertible), and tamper evident, they offer a broad and versatile application spectrum. Optical strong PUFs enable remote authentication of both objects and data.^{48,58} Protocols and systems have been proposed and demonstrated for their applications in encryption and secure communication.^{59–62}

G. Weak PUFs and unique objects

Optical weak PUFs are another form of storing secret keys in a vulnerable optical system. In contrast to strong PUFs, weak PUFs have small fixed CRP libraries with a challenge–response interface that is kept access-restricted from attackers.⁶³ In addition, there are optical unique objects (UNOs),^{64,65} which are open-access fingerprints that have been developed for product authentication, tracking, and anti-counterfeiting. Almost all paper documents, plastic cards and product packaging contain a unique physical identity code formed from microscopic imperfections in the surface, which can be read from a reflected image.^{66–68} Beyond the intrinsic “fingerprint,” various disordered structures are engraved or attached to objects and function as optically readable, unforgettable tags/labels. Examples include randomly deposited plasmonic nanoparticles⁶⁹ and femtosecond laser filament-induced scattering surfaces.⁷⁰ The readout is not limited to optical scattering patterns, fluorescence patterns, or laser emission patterns provide unique responses as well. Examples are excitation-selected lanthanide luminescence from zeolites dispersed in polymer films,⁷¹ random nanowire arrays with size-dependent dual lasing emission.⁷²

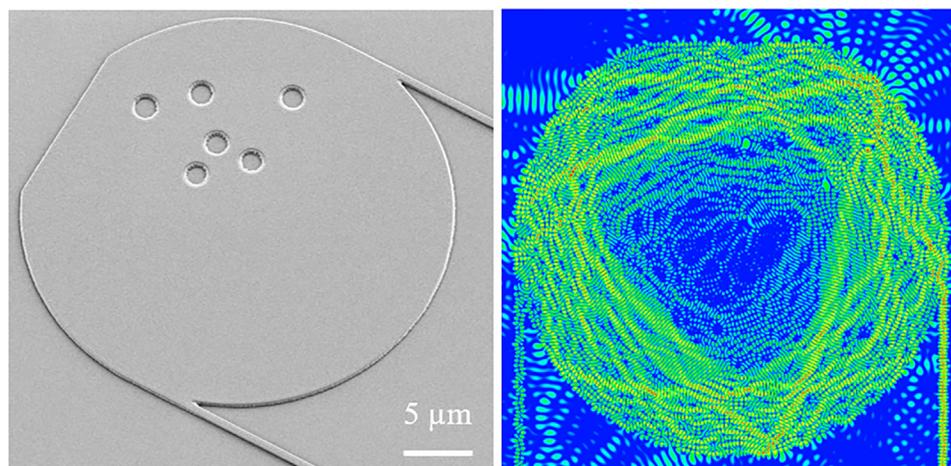


FIG. 6. Nonlinear optical PUF for enhanced security. Reprinted with permission from Grubel *et al.*, *Opt. Express* **26**, 4710 (2018). Copyright 2018 The Optical Society. (Left) Scanning electron microscope (SEM) image of a two-dimensional optical cavity with input and output waveguides fabricated in a silicon wafer. The cavity boundary shape introduces chaotic ray dynamics and the randomly positioned air holes inside the cavity cause light scattering. (Right) Simulated intensity distribution in the cavity, created by an input pulse, revealing chaotic ray dynamics. The short pulse induces optical nonlinearity inside the cavity, increasing the complexity of the response. While the challenge is encoded in the input spectrum modulation, the response lies in the output spectrum.

Edible photonic UNOs made of fluorescent biomaterials, which can be directly attached to the surface of medicines, are proposed for pharmaceutical anti-counterfeiting.⁷³

III. RANDOM LENS

In this section, disorder is intentionally introduced for optical imaging and light focusing to enhance the spatial resolution and the field of view. After a brief introduction of random lens imaging (Sec. III A), we describe its transfer function for coherent and incoherent illumination (Sec. III B). The random lens often combines with compressive sensing or machine learning for image recovery, as detailed in Sec. III C. Without calibration of its transfer function, random lens has been used for imaging based on cross-correlation or auto-correlation (Sec. III D). In addition, reference-free holographic imaging and wavefront sensing are realized with pseudo-random masks or thin diffusive layers (Sec. III E). Furthermore, light focusing by a random lens in combination with a spatial light modulator can enhance the spatial resolution of fluorescence microscopy (Sec. III F). The imaging techniques developed with random lens are adopted to multimode optical fibers with uncontrolled mode/polarization mixing and disordered fibers for endoscopic imaging (Sec. III G).

A. Lens imaging

A conventional lens, designed for two-dimensional (2D) imaging, focuses light from one point on the object plane to a point on the image plane [Fig. 7(a)]. The spatial resolution is determined by the angular range θ_{max} of light that is captured by the lens, which corresponds to the numerical aperture (NA) of the lens. The field of view (FOV) depends on the lateral dimension of the sensor area of the

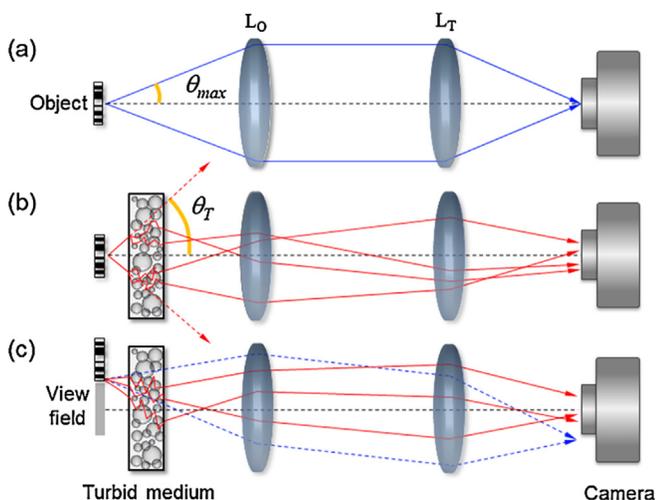


FIG. 7. Conventional lens vs random lens. Reprinted with permission from Choi *et al.*, Phys. Rev. Lett. **107**, 023902 (2011). Copyright 2011 The American Physical Society. (a) Conventional imaging with an objective (L_O) and a tube (L_T) lenses. θ_{max} is the maximum angle of light captured by the objective lens, which determines the spatial resolution. (b) After inserting a disordered medium, the waves of original angle θ_T exceeding θ_{max} can be captured after being scattered and redirected, so spatial resolution is enhanced. (c) The field of view (FOV) is also increased by scattering, as some of the scattered waves from an object outside the conventional FOV will reach the camera.

camera as well as the image magnification. Such a lens faces a trade-off between the spatial resolution and the field of view. As the diffraction-limited resolution increases with the NA of the lens, the field of view shrinks.

A random lens,⁷⁴ also called opaque lens,⁷⁵ turbid lens,⁷⁶ scattering lens,⁷⁷ or diffuserCam,⁷⁸ is an unconventional imager comprised of a disordered structure. As schematically illustrated in Fig. 7, incorporating a random scattering medium to an imaging system brings several advantages.⁷⁶ First, the spatial resolution is enhanced by an effective increase in the NA, since light emitted from the object at large angles that would miss the camera can be redirected by the random lens back to the camera [Fig. 7(b)]. Second, the field of view is enlarged, because light from any point on the object is scattered into many directions, and some of which will reach the camera [Fig. 7(c)]. Third, volumetric (3D) imaging is possible with a planar (2D) sensor array, as objects at different axial planes will generate distinct scattering patterns at the sensor plane.⁷⁹

The typical image projected by a random lens onto a camera is a seemingly random pattern with little resemblance to the object. Computational models and algorithms, based on compressive sensing and machine learning, must be employed for random lens calibration and image reconstruction. The quality of reconstructed images relies heavily on algorithms that shift the burden from the hardware to software and make the imaging system much cheaper. The lenses comprised of disordered structures not only reduce the hardware cost, but also expand the space of imaging system designs and add novel imaging functionalities.

A closely related topic is imaging through random scattering media, which has attracted much attention and investigation in recent years.^{17,27–31} These studies aim to mitigate the effects of unwanted scattering that scrambles the image. In contrast, random lenses exploit disorder and scattering for focusing and imaging applications. Their implementations benefit from techniques and algorithms developed for imaging through random media.

B. Transfer function

Depending on the coherence of illuminating light and the response of an object, optical imaging is either coherent or incoherent. With the many-to-one mapping of a random lens, light from different positions of an object can reach the same pixel of the camera. If the fields are mutually incoherent, their intensities will be added, and the transfer function relates the intensity distribution over the camera to every point across the object. However, if the fields from the object are coherent, they will interfere on the camera, and the transfer function maps the field from the object to the camera.

1. Coherent imaging

The transfer function of a random lens \mathbf{M}_F maps the field distribution across an object $\mathbf{E}_{in}(\mathbf{r})$ to that over a camera $\mathbf{E}_{out}(\mathbf{r})$,

$$\mathbf{E}_{out}(\mathbf{r}) = \mathbf{M}_F \cdot \mathbf{E}_{in}(\mathbf{r}). \quad (3)$$

\mathbf{M}_F is a complex matrix of dimension $N_o \times N_i$, where N_i and N_o denote the number of input and output channels. For a conventional lens, \mathbf{M}_F is a diagonal matrix; but for a random lens, its off-diagonal elements do not vanish. After \mathbf{M} is calibrated, the field distribution across an object can be reconstructed from the measured field pattern

on the camera:⁷⁶ $\mathbf{E}_{\text{in}} = \mathbf{M}_{\text{F}}^{-1} \cdot \mathbf{E}_{\text{out}}$. However, the matrix inversion $\mathbf{M}_{\text{F}}^{-1}$ is unstable in the presence of noise. Tikhonov regularization is applied to obtain an approximate solution.⁸⁰ The image reconstruction can be further improved by illuminating the object with different wavefronts⁸¹ or increasing the number of detected channels.⁸⁰

To reach a sub-wavelength resolution, a random lens made of closely packed nanoparticles is placed in close proximity of an object.⁸² The evanescent waves from the object, which carry high spatial frequency components, are converted to propagating waves via scattering with nanoparticles in the random lens, and sub-wavelength resolution is achieved with far-field detection. The near-field to far-field transfer function is calibrated using the near-field scanning optical microscope (NSOM).

2. Incoherent imaging

If an object is illuminated by spatially incoherent light or it produces an incoherent signal such as fluorescence upon coherent excitation, the transfer function that maps *intensity* distribution from the object to the camera is a real, positive matrix. The first implementation of a random lens is a disordered array of small mirrors,⁷⁴ and the transfer function is modeled by geometric ray optics. The random lens is also combined with a pinhole camera for sparkle vision.^{83,84} While a diffusive layer can provide a larger angle of light collection via multiple scattering, the low transmission leads to a poor signal to noise ratio (SNR). Thin diffusers or random phase masks have much higher transmission and better SNR. Moreover, they possess a larger range of the memory effect.

Because of the angular memory^{85,86} (intrinsic isoplanatism), a lateral displacement of a point source will not change the scattering pattern but only translate it laterally at the sensor plane [Fig. 8(a)]. The point spread function (PSF) $P(\rho', z'; \rho, z)$ describes the intensity distribution on the sensor array (ρ', z') generated by a point source at (ρ, z) . z denotes the distance from the source to the random lens, and z' from the lens to the sensor. With the origins of transverse coordinates ρ and ρ' on the z -axis, the angular memory effect is expressed as

$$P[\rho' - (z'/z) \Delta\rho, z'; \rho + \Delta\rho, z] = P(\rho', z'; \rho, z). \quad (4)$$

Furthermore, an axial shift of the point source rescales the PSF in the case of single scattering (light is only scattered once by the random lens), as shown in Fig. 8(b). Such memory effects greatly simplify the PSF calibration process.⁷⁸

Since any object can be considered as a sum of point sources $O(\rho, z)$, the detected intensity distribution is a convolution of the object with the PSF,

$$I_{\text{det}}(\rho', z') = \int O(\rho, z) P(\rho', z'; \rho, z) d\rho dz \equiv O * P, \quad (5)$$

where $*$ denotes the convolution operation. The deconvolution with known PSF reconstructs a 3D object from a 2D image. Although the raw data are collected on a fixed sensor grid, one can choose a nonuniform 3D reconstruction grid arbitrary. This choice is crucial for efficient reconstruction without resolution loss.⁷⁸ In contrast to the traditional imaging system whose resolution is independent of the scene, the image reconstruction using nonlinear algorithms may degrade the effective resolution as the scene complexity increases. As a result, the two-point resolution is often better than the multi-point resolution.

While the above expressions are given for incoherent imaging, a similar expression can be obtained for coherent imaging by replacing the intensity with a complex field.

C. Compressive sensing and machine learning

The random lens may be regarded as a parallel implementation of the single-pixel camera developed for compressive sensing, as illustrated in Fig. 9. In the field of compressive imaging, pseudo-random masks have been extensively used to sample objects, because they are uncorrelated with any mathematical basis in which the object images have sparse representations. In contrast to the single-pixel camera which projects the signal from an object onto different pseudo-random masks sequentially, the random lens enables simultaneous projections onto multiple camera pixels in a single acquisition.

Compressive sensing algorithms allow image reconstruction of sparse objects, when the number of sensors is significantly smaller than the number of sampling points on the object.^{78,79,81} The compression ratio depends on the relative sparsity of the object.⁸¹ Such compression is essential to achieve volumetric imaging of a 3D object with a 2D detector array.⁷⁸

Machine learning has recently been applied to imaging through scattering media and light control.⁸⁷⁻⁹⁴ The main goal is to “learn” the transfer functions of unknown structures in the presence of noise.^{95,96} Such learning can make the random lens robust against external perturbations that modify the transfer function, avoiding frequent recalibration.

D. Correlation-based imaging

To skip the transfer function characterization, correlations among scattered waves have been employed for imaging with a random lens of unknown structure. Starting with the initial proposal of a “wall lens,”^{97,98} several schemes have been proposed and realized over the years.

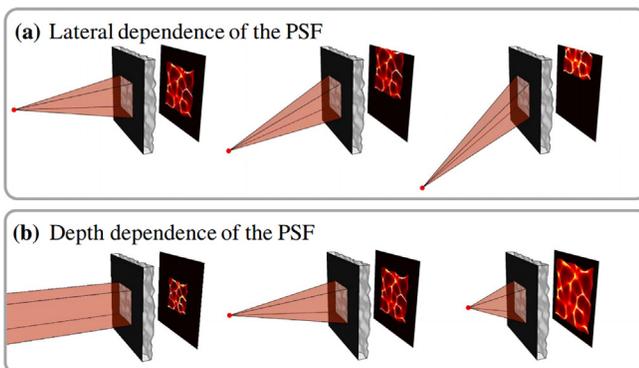


FIG. 8. Point spread function (PSF) of scattering lens. Reprinted with permission from Antipa *et al.*, *Optica* **5**, 1 (2018). Copyright 2018 The Optical Society. The PSF is given by the far-field intensity pattern created by light from a point source propagating through a thin scattering layer. (a) The PSF translates laterally as the point source shifts in the lateral direction. (b) The PSF rescales as the point source moves in the axial direction. Such effects greatly simplify the PSF calibration process of a thin scattering lens.

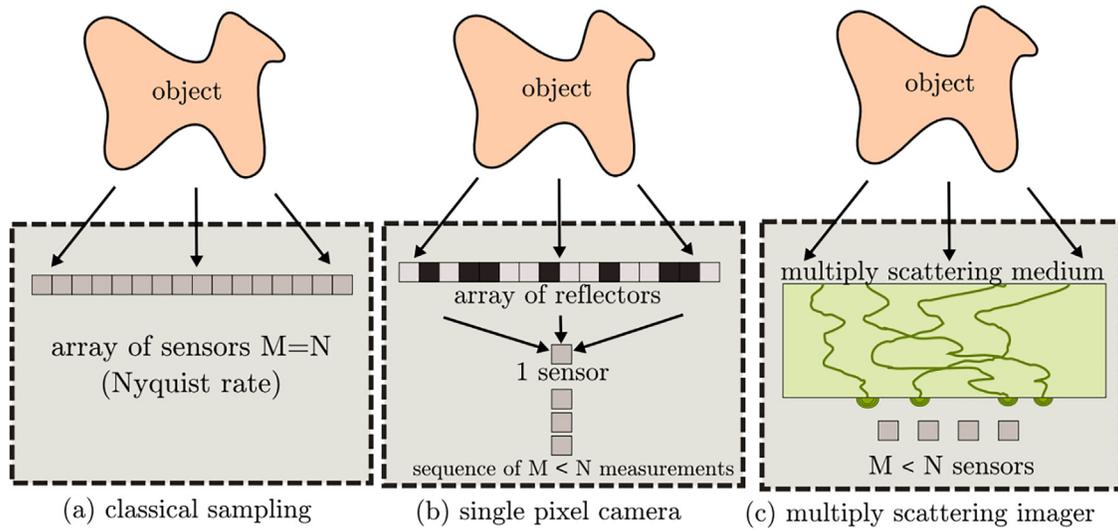


FIG. 9. Compressive imaging with random lens. Reproduced with permission from Liutkus *et al.*, *Sci. Rep.* 4, 5552 (2014). Copyright 2014 Author(s); licensed under a Creative Commons Attribution (CC BY) license. (a) Classical Nyquist–Shannon sampling: waves originating from an object of size N are captured by an array of $M = N$ sensors. (b) Single-pixel camera: an object is sampled by M successive random projections onto a single sensor using a digital multiplexer. (c) Imaging with a random lens: M sensors simultaneously capture different random projections of the original object. In (b) and (c), sparse objects can be reconstructed with $M < N$.

1. Cross-correlation

The first method utilizes the correlation between the random lens output from a reference wave and that from the signal to recover the object. The reference wave is not necessarily coherent with the

signal from the object.^{97,98} As illustrated in Fig. 10(a), a point source at (ρ, z) serves as the reference, its spherical wavefront impinges on the random lens (a scattering layer), and the transmitted or reflected intensity distribution provides the PSF, $P(\rho, z; \rho', z')$. It is then correlated with the intensity distribution $I_{det}(\rho', z')$ created by an object

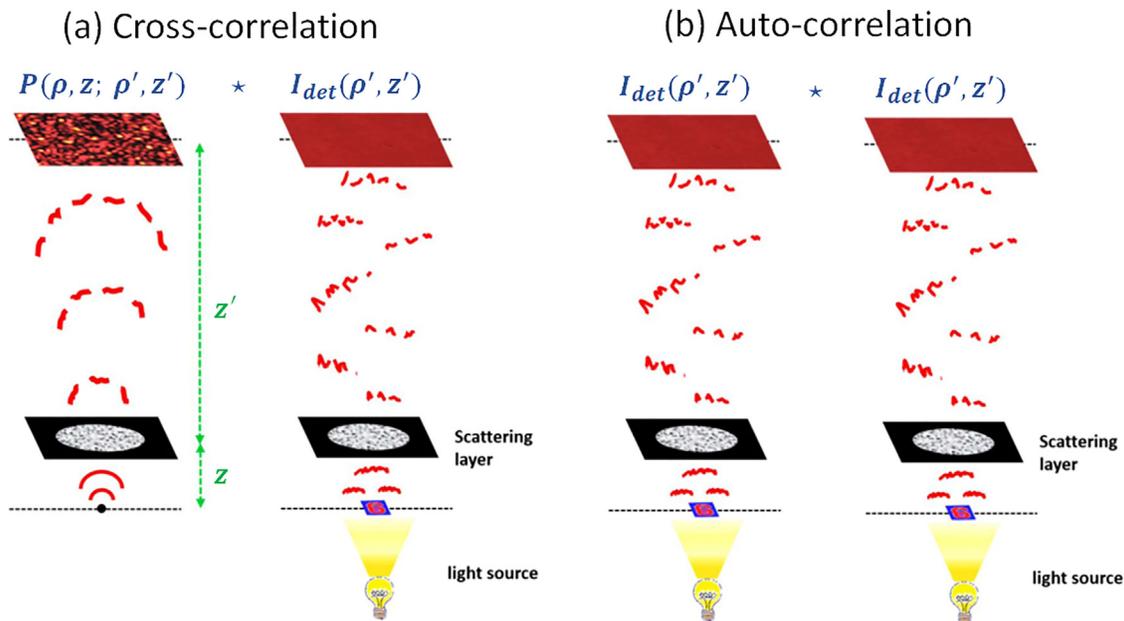


FIG. 10. Correlation-based imaging with random lens. Reproduced with permission from Singh *et al.*, *Sci. Rep.* 7, 10687 (2017). Copyright 2017 Author(s); licensed under a Creative Commons Attribution (CC BY) license. (a) Cross-correlation between the point spread function (PSF) created by a point source, $P(\rho, z; \rho', z')$ and the image of an object through a thin scattering layer, $I_{det}(\rho', z') = O * P$, recovers the object $O(\rho, z)$ [see Eq. (6)]. (b) Auto-correlation of $I_{det}(\rho', z')$, $I * I$, is equal to $O * O$, from which O is retrieved [see Eq. (7)].

$O(\rho, z)$. Although the reference wave and the object wave do not interact directly, they interact indirectly via the random lens. Since I_{det} is the convolution of the object O and the PSF P , the cross-correlation between I_{det} and the reference P gives

$$I_{\text{det}} \star P = (O \star P) \star P = O \star (P \star P) = O, \quad (6)$$

where \star denotes the correlation operation, and the auto-correlation of the PSF ($P \star P$) can be approximated by a Dirac delta function δ whose convolution with O gives O .

In principle, the volumetric image of a 3D object can be constructed from the cross-correlation of 3D intensity distributions generated by the random lens with the reference source and the object separately. In reality, a 2D sensor array is often used to record the intensity distribution on a single plane. From it, a sharp image of a 2D object or cross section of a 3D object with distance to the random lens z_{obj} equal to that of the reference source to the lens z_{ref} is retrieved.⁹⁹ The random lens satisfies the same imaging condition as a conventional lens: $1/z + 1/z' = 1/f$, where $z = z_{\text{obj}} = z_{\text{ref}}$ is the working distance from the object to the random lens, $z' = z_{\text{det}}$ is the distance between the detector plane and the random lens, and f is the effective focal length.^{97,98} While a conventional lens has a fixed focal length, the random lens has an adaptive focal length that adjusts itself for arbitrary chosen z and z' . The lateral magnification $m = -z'/z$ is independent of wavelength λ , even though the transmitted/reflected intensity pattern changes with λ . Hence, the magnification can be increased by moving the random lens away from the detector toward the object. The lateral resolution is given by $\text{RES} \simeq 1.22\lambda z/D_a$, where D_a is the diameter of the input aperture on the random lens. By bringing an object closer to the random lens or by increasing the aperture diameter, RES decreases and the resolution is enhanced.

The field of view (FOV) is limited by the range of angular memory effect.^{97,98} If light transport in the random lens is diffusive, $\text{FOV} \simeq \lambda z/\pi L_s$, where L_s is equal to the thickness of the lens when operating in the transmission mode or the transport mean free path in the reflection mode. The FOV depends on the working distance z from the object to the random lens. The depth of field DOF is proportional to $\lambda(z'/D_a)^2$ and is independent of the working distance z .⁹⁹ Similar to a conventional lens, the random lens has a trade-off between the lateral resolution RES and the field of view FOV: $\text{FOV}/\text{RES} \sim D_a/L_s$. However, this trade-off is achromatic with no dependence on wavelength.

2. Auto-correlation

While it does not require the calibration of a random lens, cross-correlation-based imaging does require a known reference, which may not be possible in some cases. An auto-correlation method, originally invented for noninvasive single-shot imaging through scattering medium,^{100,101} is adopted for random lens imaging without a reference. Let us consider incoherent imaging with a random lens, $I_{\text{det}} = O \star P$, in Fig. 10(b). The auto-correlation of I_{det} is equal to the auto-correlation of the object O ,

$$I_{\text{det}} \star I_{\text{det}} = (O \star P) \star (O \star P) = (O \star O) \star (P \star P) = O \star O. \quad (7)$$

The Fourier transform $\mathcal{F}\{I_{\text{det}} \star I_{\text{det}}\} = \mathcal{F}\{O \star O\} = |\mathcal{F}\{O\}|^2$ gives the amplitude of Fourier transform of O , $|\mathcal{F}\{O\}|$. The phase of

$\mathcal{F}\{O\}$ can be retrieved numerically, under the object constraints. The reconstructed $\mathcal{F}\{O\}$ gives O via an inverse Fourier transform.

Typically, the phase retrieval algorithms work efficiently for sparse objects. However, for objects with large size, low sparsity, and high complexity, the image contrast is low, as I_{det} is an incoherent sum of many shifted PSF. The low contrast restricts the size and complexity of the object that can be reconstructed using a phase-retrieval algorithm. To circumvent this difficulty, a reference point source is added to the scene:^{102,103} $O(\rho) + \delta(\rho - \rho_0)$. Unlike the cross-correlation method described above, there is no need to measure the random lens output when illuminated only by the point source (without the object). The autocorrelation of random lens output I_{det} , taken with both the object and the reference present, gives two spatially offset copies of the object, $O(\rho - \rho_0)$ and $O(\rho + \rho_0)$. This method permits direct reconstruction of the object without phase retrieval.

E. Holographic imagers and wavefront sensors

In parallel to random lens developments, pseudo-random masks are adopted in reference-free holographic imaging, also called phase imaging.^{104–110} Unlike most random lens, the amplitude or phase pattern of a mask is usually known by design and its transfer function can be predicted. To probe the phase front from the intensity measurement, light from an object is diffracted by the mask, and the interference of waves from different positions on the phase front produces intensity modulations. This step encodes phase information into intensity variation. The transmitted/reflected intensity patterns are recorded at one or several planes, from which the incident field to the mask is reconstructed. While recording multiple intensity patterns at different planes guarantee a unique, accurate, and fast-convergent reconstruction, single-plane recovery is possible for sparse objects. The “randomness” in the mask (aperture) eliminates any possible symmetry or degeneracy in the interference pattern, thus avoiding stagnation or ambiguity in the phase recovery.

Since the phase-retrieval is an iterative process, it takes time to converge, posing a challenge for real-time imaging and tracking. To address this issue, the intensity pattern without any object is recorded first, and then, the change of pattern caused by insertion of an object is used for full-field (amplitude and phase) reconstruction in a single (non-iterative) processing step.¹⁰⁷

In addition to pseudo-random masks, a thin diffusive layer with an unknown internal structure has been used for holographic imaging.^{111,112} Its scattering matrix is first calibrated and then correlated with the speckle intensity pattern of an unknown signal passing through the diffusive layer. Finally, the full field of the signal is recovered from the correlation. This technique enables high-resolution holographic imaging with a long working distance beyond what a conventional objective lens can achieve.¹¹³

An alternative way of wavefront sensing using a thin diffuser is to place it in the close vicinity of a camera.¹¹⁴ The diffuser produces a speckle pattern that is recorded by the camera. Due to the angular memory effect, the speckle grains in the camera are translated with the incident wavefront tilt. The local wavefront gradient can be determined from the local translation of the speckle pattern. The translation vector map is computed with a fast diffeomorphic image registration algorithm and then integrated to reconstruct the entire wavefront. While a change of the wavefront is efficiently converted to a change in the speckle pattern, the exact intensity distribution depends on the

unknown structure of the scattering layer. Nevertheless, the correlation between two incident wavefronts is directly related to the correlation between their speckle patterns produced by the scattering layer, independent of the scattering structure of the layer.¹¹⁵ This universal relation facilitates wavefront sensing with arbitrary diffusers.

F. Light focusing and fluorescence microscopy

Another imaging modality is focusing the probe beam by a lens to an object and collecting the response signal while scanning the focal spot across the object. This can also be done with a random lens, but requires a spatial light modulator (SLM) to pre-compensate the wavefront distortion of the probe beam by scattering.^{116,117} As shown in Fig. 11, a smaller focal spot is obtained when inserting a multiple-scattering slab between a conventional lens and a camera, as the large-angle scattering effectively increases the numerical aperture.⁷⁵ To further reduce the focal spot size, an annular mask is placed after the random lens to filter low spatial frequency components in the transmitted field.¹¹⁸ Also, a random lens is constructed with high refractive-index material to focus down to sub-100 nm.¹¹⁹ In addition to focusing in the far-field, near-field focusing is possible with a lens made of disordered nanoparticles.¹²⁰

Thanks to the angular memory effect, once the incident wavefront for focusing to a particular position is found, the focal spot can be scanned laterally by tilting the wavefront. Similar to correlation-based imaging, there is a trade-off between the scanning range (field of scan) and the spatial resolution (size of focus). It is possible to overcome this trade-off, that is, to reach beyond the memory effect range, by calibrating the field transfer function of the random lens, which provides the incident wavefront for focusing to any point or even multiple points.¹²¹ Even if only a subset of the matrix is measured, a

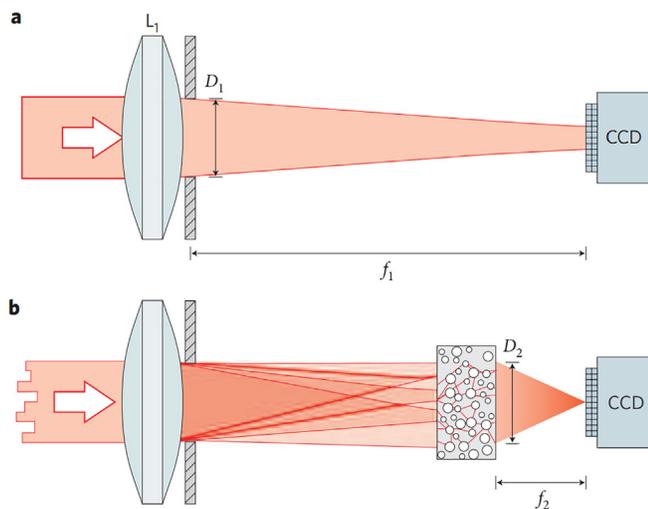


FIG. 11. Disorder improves light focusing. Reprinted with permission from Vellekoop *et al.*, *Nat. Photonics* **4**, 320 (2010). Copyright 2010 Nature Publishing Group. (a) A conventional lens L_1 with focal distance f_1 focuses light onto a camera. An iris controls the aperture D_1 of the lens. The focus is as sharp as the diffraction limit of the lens. (b) A disordered sample at distance f_2 from the camera randomly scatters the light. After shaping the incident wavefront with a spatial light modulator (not shown), the light focuses through the scattering sample to a spot that is smaller than that in (a). D_2 is the diameter of the diffuse spot at the back of the sample.

technique called sparse field focusing allows arbitrary scanning of the focus, but with lower contrast.¹²²

Typically, a bulk random lens has a statistically isotropic structure. Recently, the random lens with anisotropic scattering structure is fabricated and used in combination with a SLM to focus light to submicrometer-thin sheets.¹²³ Furthermore, a disorder-engineered metasurface is designed and fabricated. Thanks to its extremely broad scattering range, light can be focused to 10^8 points.¹²⁴

In addition to the structural design of random lens, the point spread function (PSF) can be engineered by numerical processing of the transfer function. For example, by numerically applying a Fourier filter to the transmission matrix of a random lens, the 3D profile of its focus is shaped at will.¹²⁵ Bessel, donut, and helical beams are generated, as well as foci smaller than the diffraction-limited speckle size.

Disordered metallic nanostructures have been utilized to construct plasmonic lens for near-field focusing with far-field control.¹²⁶ By coupling the wavefront-shaped far-field optical waves ($\lambda = 637$ nm) to a 2D random array of holes in a thin gold film, surface plasmon polaritons can be focused to arbitrary positions with a spot size of 170 nm. Hence, the plasmonic random lens may be applied to near-field focusing and scanning microscopy with sub-wavelength resolution.¹²⁷

One issue of focusing waves with a random lens is the non-zero background outside the focus. Although the intensity at the focus can be much higher than the average intensity of the background, the energy inside the focus is still much lower than the total energy outside. Another issue of using the random lens is that a SLM is needed to shape the incident wavefront of a coherent beam for focusing. To overcome these issues, a technique has been invented for fluorescence imaging through a scattering medium without a SLM.¹⁰⁰ An unknown speckle pattern generated by a laser beam propagating through a random medium illuminates a thin sample, and the fluorescence signal produced by the speckled illumination is measured by a bucket detector. Then, the illuminating speckle pattern is raster-scanned across the sample by tilting the incident laser beam onto the random medium. From the fluorescence signals recorded for a range of angles within the memory effect range, a 2D image of the sample is reconstructed. This technique is adopted for fluorescence imaging with a high-index random lens to enhance the spatial resolution to 116 nm.¹²⁸ To image beyond the range of angular memory effect, additional low-resolution fluorescence images are taken for reconstruction of a wide field of view.

G. Multimode fiber endoscopy

Although a bundle of single-mode optical fibers has been widely employed for endoscopic imaging, it is advantageous to use a multimode fiber (MMF),^{129–132} because its larger NA gives better resolution and its smaller cross section means less invasive. The higher areal density of optical guided modes in a MMF enhances the information capacity. However, the fiber modes have different propagation constants and acquire varying phase delays, and thus, spatial images transmitted through a MMF will be distorted. Moreover, random coupling of guided modes, caused by fiber imperfections and external perturbations, further scramble the information, similar to the process of light scattering in a disordered material. Hence, a MMF with uncontrolled mode coupling resembles a random lens. Its transfer function maps the input fields in all fiber modes to the output field distribution in an

object plane.^{133–135} After calibration of the transfer function, the field patterns at the fiber distal end can be recovered from the signals transmitted back to the proximal end.^{136–139} Machine learning and compressive sensing techniques have been used for image classification and reconstruction through MMFs, which are robust against environmental changes and wavelength drift.^{140–157}

Similar to random scattering medium, it is possible to focus light or create arbitrary spatial pattern at the fiber output by shaping the input wavefront of a laser beam.^{133,158–166} In short fibers with weak mode coupling, rotational and quasi-radial memory effects allow transverse scanning of a focal spot.^{167–169} If light propagates through a MMF with a specific propagation constant, a quadratic radial phase modulation of the input wavefront will cause an axial shift of the output pattern.¹³⁶ More recently, the translational memory effect is observed in MMFs with a square cross section.¹⁷⁰ However, none of these memory effects will survive in long MMFs with strong mode coupling. To increase the spatial resolution of 3D imaging and optical manipulation, photonic crystal fibers with numerical aperture significantly higher than that of conventional fibers are used.^{171,172} Alternatively, a highly scattering material is added to the distal end of a MMF to enable the formation of smaller foci at longer distances from the fiber tip.¹⁷³ Instead of shaping the input wavefront, the transfer function of a MMF can be modulated by applying computer-controlled mechanical perturbations to the fiber to obtain desired output patterns.¹⁷⁴

Using a minimally invasive MMF, subcellular spatial resolution has been achieved for deep-brain *in vivo* imaging.^{175,176} Optical sectioning and enhanced resolution are demonstrated with saturated excitation and temporal modulation.¹⁷⁷ Compared to one-photon excitation, two-photon excitation through a MMF improves depth sectioning for 3D fluorescence imaging.¹⁷⁸ To enhance the image contrast, digital confocal microscopy through a MMF is realized by digitally engineering the excitation wavefront and then applying a virtual digital pinhole on the collected signal.¹⁷⁹ To acquire chemical contrast for diagnosis, nonlinear microscopy based on coherent anti-Stokes Raman scattering (CARS) is developed with a MMF endoscope.¹⁸⁰ Hybrid photoacoustic-fluorescence microendoscopy through a MMF is shown to provide both anatomical and functional contrasts.¹⁸¹ Beyond the imaging applications, 3D printing at the distal end of a MMF is demonstrated by wavefront shaping of input laser pulses.¹⁸²

While conventional optical fibers are mostly used for convenience, disordered fibers are fabricated and exploited for endoscopic imaging^{183–187} and information transmission.¹⁸⁸ The refractive index fluctuates randomly over the fiber cross section, but remains uniform along the fiber.¹⁸⁹ Transverse scattering and interference results in transverse localization of light, similar to Anderson localization in a 2D disordered structure. Such fibers can transport transversely localized beams with low crosstalk.¹⁹⁰ It has been shown that the transported images have less pixelation and higher contrast than those through the multicore fibers.^{183,184}

IV. SPECKLE-BASED SPECTROMETERS

In this section, optical speckles, generated by random scattering structures or multimode fibers, are utilized to build compact spectrometers with record-breaking resolution. After introducing relevant parameters for spectrometers (Sec. IV A), we describe three

mechanisms underlying speckle spectrometers and wavemeters: random optical diffraction (Sec. IV B), multiple light scattering (Sec. IV C), and multimode waveguide/fiber dispersion (Sec. IV D). Finally, we will discuss the pros and cons of computational spectrometers based on speckle and disorder (Sec. IV E).

A. Spectrometer parameters

Optical spectrometers are widely used in scientific and industrial research. The performance of a spectrometer is characterized by multiple parameters. The spectral resolution $\delta\lambda$ denotes the smallest difference in wavelength λ that can be distinguished. The resolving power is the ratio of wavelength λ and resolution $\delta\lambda$. The finesse is given by the number of spectral channels N_λ that can be covered in one measurement. Each spectral channel has a width of $\delta\lambda$. If these channels are contiguous in wavelength, the wavelength range covered in one acquisition equals to $N_\lambda \Delta\lambda$. The free spectral range (FSR) denotes the minimal spacing of (well-separated) wavelengths at which a spectrometer produces identical response, and limits the spectral bandwidth of a spectrometer.

The sensitivity of a spectrometer depends on the photon throughput, that is, the percentage of photons entering the spectrometer eventually reaching the sensors. How weak a signal that a spectrometer can measure depends not only on the signal strength but also on the amount of detection noise, ultimately the signal-to-noise ratio (SNR). The signal strength increases with collection efficiency, which is related to the number of spatial modes a spectrometer can harvest while maintaining the spectral resolution. For many applications, the operation speed matters, and it determines the number of spectra that can be measured or reconstructed in a second. Finally, size, weight, power, and cost (SWaP-C) are also relevant parameters for practical applications.

Most spectrometers face tradeoffs between some of aforementioned parameters. For example, a grating spectrometer diffracts light of different wavelengths to different directions. Two closely wavelengths, which have slightly different diffraction angles, can only be spatially separated and measured by different detectors after propagating over a long distance L from the grating to the detector. The spectral resolution $\delta\lambda$ scales as $1/L$, so a smaller spectrometer has lower resolution. The trade-off between resolution and size limits the performance of chip-scale spectrometers—a key element for low-cost, portable sensing and lab-on-a-chip applications, hence prompting exploration of alternative mechanisms for spectrometer operation. As will be shown below, incorporating disorder into spectrometers not only overcomes the trade-off between size and resolution, but also removes other limitation like the free spectral range.

B. Random optical diffraction

With randomized width or depth of grooves, a disordered grating, also called a random polychromat,¹⁹¹ diffracts light of one wavelength to many directions [Fig. 12]. The one-to-many spectral-to-spatial mapping is characterized by a point spread function, $P(x; \lambda)$, which describes the spatial intensity distribution of diffracted light at wavelength λ . Because waves of different λ do not interfere in the time-integrated measurement, their intensities add at each sensor. The intensity distribution over a sensor array $I_{\text{dif}}(x)$ is related to the spectral density of an input signal $I_{\text{sig}}(\lambda)$ by $P(x; \lambda)$,

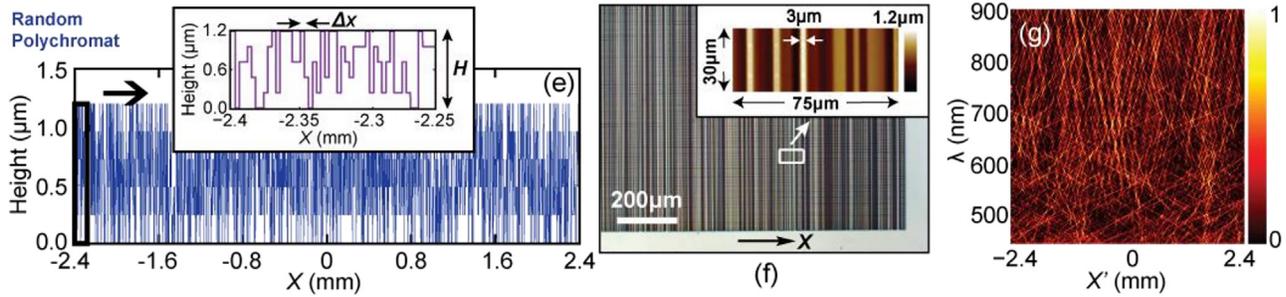


FIG. 12. Random polychromat (disordered grating) for spectrum reconstruction. Reprinted with permission from Wang *et al.*, Opt. Express **22**, 14575 (2014). Copyright 2014 The Optical Society. Left panel: Depth profile showing random fluctuation of groove depth of a grating. Inset is magnified view of a segment enclosed by the black box. Middle panel: Optical micrograph of a corner of the fabricated random polychromat. Inset shows atomic-force microscope measurement of a small region delimited by the white box. Right panel: Spatial-spectral PSF $P(x; \lambda)$ measured at a distance of 450 mm from the random polychromat. The spectral resolution is 1 nm.

$$I_{\text{dif}}(x) = \int P(x; \lambda) I_{\text{sig}}(\lambda) d\lambda. \quad (8)$$

Once $P(x; \lambda)$ is calibrated by recording the diffraction patterns at individual wavelengths using a tunable source, any unknown spectrum $I_{\text{sig}}(\lambda)$ can be recovered from the measured diffraction pattern $I_{\text{dif}}(x)$.^{191,192} However, the spatial profile and polarization state of a signal incident onto the random polychromat must be identical to those adopted in the PSF calibration. Also, the distance L from the random polychromat to the sensor array is fixed.

The spectral resolution is determined by how small a wavelength shift will cause a notable change in the diffraction pattern. Such a change is quantified by spectral correlation of the PSF:

$$C_S(\Delta\lambda) \equiv \frac{\langle P(x, \lambda) P(x; \lambda + \Delta\lambda) \rangle_{x, \lambda}}{\langle P(x; \lambda) \rangle_{x, \lambda} \langle P(x; \lambda + \Delta\lambda) \rangle_{x, \lambda}} - 1, \quad (9)$$

where $\langle \dots \rangle_{x, \lambda}$ denotes an average over spatial position x and wavelength λ . As $\Delta\lambda$ increases, $C_S(\Delta\lambda)$ gradually decays to zero. The half-width-at-half-maximum (HWHM) provides an order-of-magnitude estimate of wavelength resolution $\delta\lambda$. Similar to a grating spectrometer, the resolution is inversely proportional to the distance L : $\delta\lambda \propto 1/L$, and a larger polychromat with finer grooves provides a better resolution.^{191,192}

The number of spectral channels N_λ that can be recovered in a single measurement is determined by the number of independent spatial channels N_x over a sensor array. Without prior information of the signal spectrum, $N_\lambda \simeq N_x$, but if there is prior information or the spectrum is sparse, $N_\lambda \gg N_x$ is possible using compressive sensing algorithms. One advantage of the random polychromat is that the spectral channels in one measurement do not need to be contiguous in wavelength. If it is known *a priori* that the signals are located in certain wavelength regions that are disconnected, the finite number of spectral channels will be allocated only to those regions. In this way, a small number of spectral channels can effectively cover a broad wavelength range.

Switching from one-dimensional (1D) to two-dimensional (2D) diffraction further increases N_λ . For example, the PSF $P(x; y; \lambda)$ is generated by a 2D array of air holes with varying diameter^{193,194} or a frosted glass with rough surface.¹⁹⁵ The mapping from 1D spectrum to 2D space greatly enhances the number of spatial channels $N_{x,y}$, which is given by the number of speckle grains within the 2D sensor

array. A tiny wavelength shift has been detected from the speckle displacement, and a resolving power of one million for a single wavelength is demonstrated.¹⁹⁶

The multiplex spatial-to-spectral mapping offered by a random polychromat is ideally suited for compressive spectroscopy. This scheme is equivalent to parallel projection of an input spectrum to multiple sensors. The one-to-many spectral-to-spatial mapping allows a small sensor array to capture light of all wavelengths without rotating the random polychromat. However, such mapping raises concerns about the SNR, because even monochromatic light spreads over many sensors, while a grating diffracts the light to a single sensor. If the signal is weak or the sensor noise is large (e.g., at the infrared wavelength), dividing the signal over many sensors is detrimental to spectrum reconstruction.¹⁹⁷ However, if the signal shot noise dominates over the sensor dark noise, the spectrum reconstructed from a random diffraction pattern has comparable quality to that measured by grating diffraction. Quantitatively, how the noise propagates through the nonlinear optimization process to manifest as an error of spectrum reconstruction is difficult to analyze.¹⁹⁷ In addition, various denoising algorithms have been developed over the years, and recent adoption of machine learning techniques significantly improves the robustness of spectrum reconstruction against measurement noise and system drift.¹⁹⁸

C. Multiple light scattering

Compared to optical diffraction from a random polychromat or single scattering by a weakly disordered material, multiple scattering in a highly disordered slab accelerates speckle decorrelation and enhances spectral resolution.³ For any dispersive medium, the spectral resolution is inversely proportional to the temporal spread of light, which is given by the optical path length difference at a single wavelength. For light diffusion in a 2D system, the optical path length distribution has a width $\Delta\mathcal{L}$ proportional to the average path length, which scales as L^2/l_t , where L is the linear dimension of the system, and l_t is the transport mean free path. The spectral resolution¹⁹⁹ is inversely proportional to the path length difference $\Delta\mathcal{L}$, which leads to the scaling $\delta\lambda \propto l_t/L^2$. Compared to the $1/L$ scaling of $\delta\lambda$ for optical diffraction and single scattering, the $1/L^2$ scaling for multiple scattering and light diffusion enables a much faster increase in resolution

with L . For the same value of L , the spectral resolution is enhanced by a factor of L/l_t , which can be much larger than 1.

However, optical diffusion reduces the transmission, as most light is reflected after multiple scattering. In the absence of dissipation, the total transmission scales as l_t/L . While the spectral resolution is enhanced by L/l_t , the photon throughput is reduced by the same factor. The trade-off between resolution and sensitivity has been addressed in the design of an on-chip spectrometer.¹⁹⁹ As shown in Fig. 13, a random array of air holes (150 nm in diameter) etched to a silicon layer is confined in a semicircle and surrounded by a highly reflecting photonic crystal boundary (periodic lattice of air holes), so that the diffusive photons are effectively channeled from an input waveguide at the base of the semicircle to the output waveguides at the circumference. While the spectral resolution is enhanced via multiple scattering of light by air holes, the throughput remains high due to suppression of reflection with the closed boundary. Although the semicircle radius is merely 25 μm , it is much larger than the transport mean free path, resulting in sub-nanometer resolution at 1500 nm wavelength.¹⁹⁹ To avoid material absorption, silicon is replaced by silicon nitride for broadband operation at visible and near-infrared wavelengths.^{200,201} Single-photon detectors and an efficient broadband fiber-to-chip coupler are integrated with the disordered structure in a

single chip.²⁰² The power sensitivity of -111.5 dBm is reached in the telecom band.

In addition to small footprint, another appealing feature for on-chip implementation is that the random spectrometer can operate over a broad wavelength range without structural modification. Regardless of input light wavelength, scattered waves always reach the sensors. The photonic-crystal boundary cannot be highly reflective at any wavelength, but it may be replaced by a random array of densely packed air holes. By adjusting the hole size and density as well as the boundary layer thickness, it is possible to reach 2D light localization, resulting in broadband reflection. In contrast to grating spectrometers, the random spectrometers do not suffer the redundancy that sets the free spectral range (FSR), because a disordered structure is free of any symmetry or degeneracy. The speckle pattern is formed by interference of numerous scattered waves going through different paths and having uncorrelated phases. The probability of having identical speckle patterns at far apart wavelengths is negligibly small, especially when the number of speckle grains is large.

One issue of the planar disordered structure is that a small amount of light is scattered out of the plane. Such loss decreases photon throughput and spectral resolution. The out-of-plane leakage is stronger for longer scattering paths, thereby preferentially attenuating

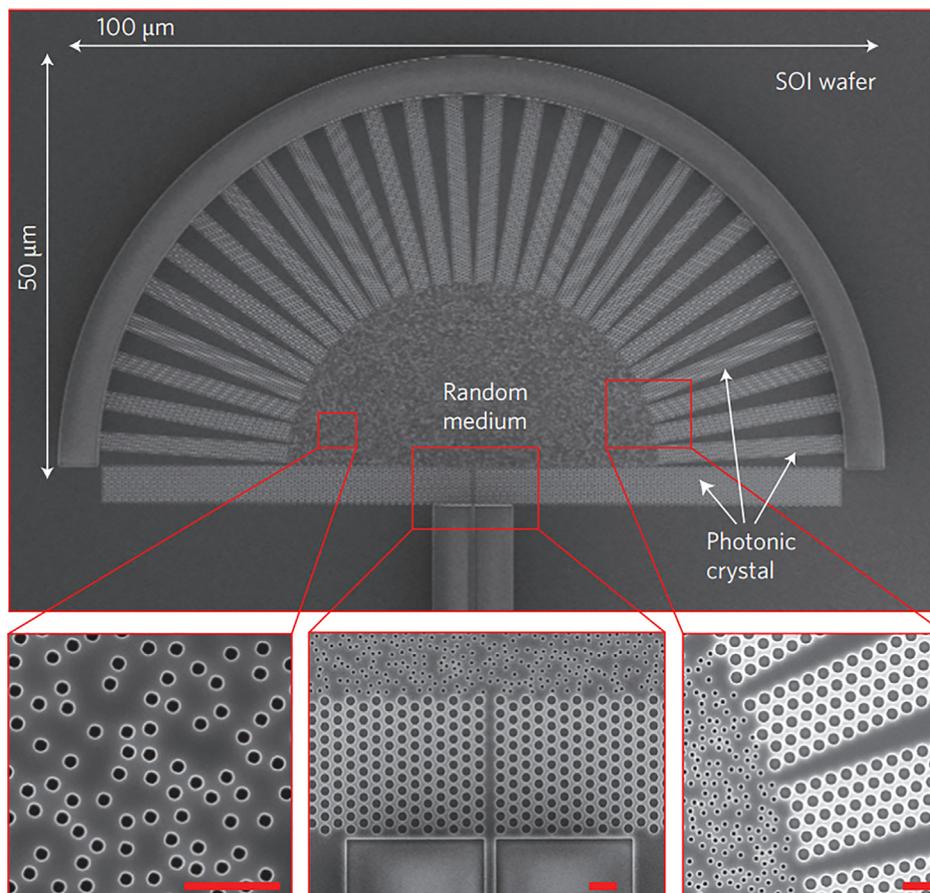


FIG. 13. Chip-scale diffusive spectrometer. Reprinted with permission from Redding *et al.*, *Nat. Photonics* **7**, 746 (2013). Copyright 2013 Nature Publishing Group. Scanning electron microscope image of a semicircular array of randomly positioned air holes in a silicon-on-insulator (SOI) wafer, surrounded by highly reflective photonic-crystal layer. The signal is launched into the random structure via a defect waveguide at the bottom of the semicircle. The light then diffuses through the random array via multiple scattering and eventually reaches the 25 defect waveguides around the circumference of the semicircle. These tapered waveguides couple the signals to photodetectors at their ends (not integrated). The distribution of intensities over the detectors is used to identify the input spectrum. The insets in the bottom row are magnified images, and the scale bars indicate 1 μm .

the light going through longer paths. The path length distribution is narrower, and the spectral resolution is lower. One way of reducing the out-of-plane scattering is engineering the spatial Fourier spectrum of a 2D scattering structure.¹⁹⁹ By introducing either short-range order or long-range order, it is possible to attenuate the spatial frequencies of the structure that facilitate out-of-plane scattering of light. Inverse design of the scattering structure can maximize the amount of light reaching the output waveguides at desired wavelengths.²⁰³ In another scheme, a thin layer of random alumina particles is inserted in between two mirrors to reduce light leakage.²⁰⁴ Principal component analysis (PCA) is applied to determine the wavelength corresponding to a speckle pattern with picometer resolution.

Integrating spheres with rough inner walls have been used for high-resolution wavelength meters (wavemeters). Light is bounced many times inside an integrating sphere, and the escaping waves interfere to form a speckle pattern at the output port. From the speckle pattern, the corresponding wavelength is identified.²⁰⁵ The wavemeter operates in the visible and near-infrared spectrum with sub-femtometer wavelength resolution. It has been exploited for laser frequency locking to an arbitrary wavelength.²⁰⁵ The maximum lock update rate of 200 Hz is limited by the time it takes to identify the wavelength using PCA. By resorting to a Poincaré descriptor of the speckle pattern, the computation time is shortened by two orders of

magnitude, enabling kHz-rate measurements of femtometer-level wavelength changes.²⁰⁶ More recently, deep learning is employed to reject instrumental and environmental noise, providing attometer-scale wavelength precision over a range of 488 nm to 976 nm.²⁰⁷ In addition to recording speckle intensity, single-shot speckle phase detection is exploited for wavelength identification with high precision.²⁰⁸

D. Multimode waveguide dispersion

A speckle pattern is also generated by a multimode fiber (MMF) through interference of light in guided modes. The transmitted field distribution at the exit face of a MMF is

$$E_{\text{MMF}}(\rho, \phi; \lambda) = \sum_{m=1}^{M_w} a_m \Psi(\rho, \phi; \lambda) e^{-i\beta_m(\lambda)L_w}, \quad (10)$$

where ρ and ϕ are polar coordinates, L_w is the fiber length, M_w is the total number of guided modes, a_m is the complex amplitude of the m -th mode whose spatial field profile Ψ and propagation constant β_m change with wavelength λ . Once the spatial wavefront and polarization state of incident light are fixed, the transmitted speckle intensity pattern, $I_{\text{MMF}}(\rho, \phi; \lambda) = |E_{\text{MMF}}(\rho, \phi; \lambda)|^2$, is unique for each wavelength

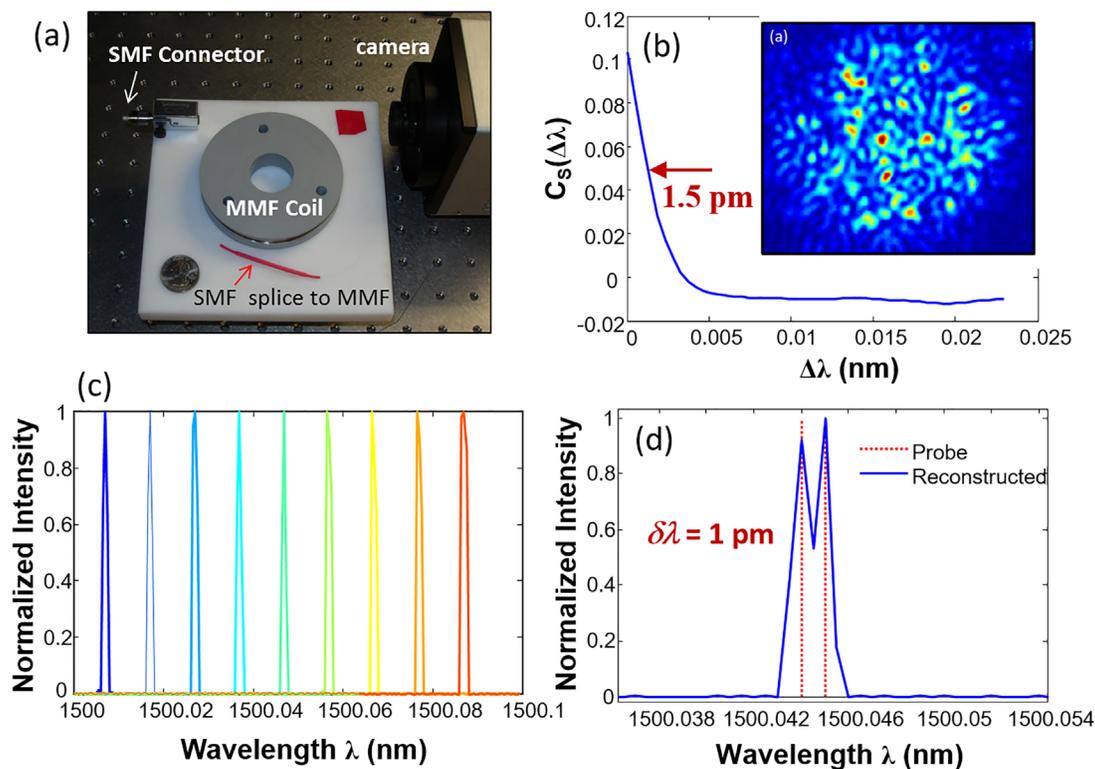


FIG. 14. Multimode fiber spectrometer with ultrahigh resolution. Reprinted with permission from Redding *et al.*, *Optica* 1, 3 (2014). Copyright 2014 The Optical Society. (a) Photograph of a multimode fiber (MMF) spectrometer. Light is coupled via a polarization-maintaining single-mode fiber (SMF) to the 100-m-long MMF (coiled to a 3 in. spool), and the transmitted speckle pattern is recorded by a monochrome camera. (b) Spectral correlation function of the speckle pattern $C_S(\Delta\lambda)$ features a half-width-at-half-maximum (HWHM) of 1.5 pm. Inset: Speckle intensity pattern measured at $\lambda = 1500$ nm. (c) Spectral lines reconstructed from speckle patterns. (d) Reconstructed spectrum (blue line) of two narrow lines separated by 1 pm. The red dotted vertical lines mark the probe wavelengths.

and serves as a fingerprint. The spectral contrast decreases as the number of spectral components increases, because their speckle patterns add incoherently. Previously, the laser linewidth has been retrieved from the speckle contrast.²⁰⁹ Recently, it is shown that the entire spectrum $I_{\text{sig}}(\lambda)$ can be reconstructed from a speckle pattern

$$I_{\text{MMF}}(\rho, \phi; \lambda) = \int P(\rho, \phi; \lambda) I_{\text{sig}}(\lambda) d\lambda, \quad (11)$$

once the PSF $P(\rho, \phi; \lambda)$ is calibrated.²¹⁰

The spectral resolution is dictated by modal dispersion that temporally stretches light through a MMF. Assuming all fiber modes are excited with equal magnitude and their coupling is negligible, the resolution is inversely proportional to the path length difference

$$\delta\lambda \propto \frac{1}{(\beta_1 - \beta_M)L}, \quad (12)$$

where $\beta_1 - \beta_M = d\beta_1/d\lambda - d\beta_M/d\lambda$ reflects the maximal difference of group delay, and it scales as NA^2 for a step-index fiber of $\text{NA} \ll 1$.²¹¹ If mode coupling is strong in a MMF, random hopping of photons among the fiber modes can be described by diffusion in the mode basis, and the path length difference is proportional to \sqrt{L} , so $\delta\lambda \propto 1/\sqrt{L}$.

Since the optical fiber has been optimized for long-distance transmission with minimal loss, a long MMF can be used to reach ultrahigh resolution without sacrificing throughput. The resolving power $\lambda/\Delta\lambda$ exceeds 10^6 for a 100-meter-long step-index MMF (core diameter $D_w = 105 \mu\text{m}$, $\text{NA} = 0.22$) at $\lambda = 1500 \text{ nm}$.²¹² Such a long fiber is coiled on a small spool, making the spectrometer (comprised of a single MMF and a monochrome camera) compact and lightweight (Fig. 14).

The MMF is also shown to function as an ultrahigh-resolution wavemeter that can precisely determine a single wavelength.²¹³ By modulating the input signal with an acoustic optical modulator (AOM) and applying the PCA, attometer resolution at $\lambda \simeq 780 \text{ nm}$ is obtained with a 18-cm-long step-index MMF ($D_w = 105 \mu\text{m}$, $\text{NA} = 0.22$). Multiple wavelengths may be resolved simultaneously by modulating them at different acoustic frequencies.²¹⁴

Since the MMF maps 1D spectrum to 2D space, a large number of spectral channels are measured in a single acquisition. As an example, a 4-cm-long MMF (core diameter = $105 \mu\text{m}$, $\text{NA} = 0.22$) covers the entire visible spectrum with 1 nm wavelength resolution in one measurement.²¹² While the fiber core diameter D_w has little influence on spectral resolution, it determines the total number of guided modes $M_w \propto D_w^2$, which sets the upper bound for the number of spectral channels N_λ . Although a large-core MMF provides a high N_λ , the speckle contrast $C_i \simeq 1/\sqrt{N_\lambda}$ is low for a dense spectrum of $N_\lambda \gg 1$. Once the contrast is below the noise level, an accurate spectrum recovery is impossible.¹⁹⁷

To overcome the trade-off between bandwidth and resolution, a wavelength division multiplexer (WDM) is integrated with a bundle of MMFs.²¹⁵ The WDM divides a broad spectrum to multiple windows, and each window is covered by a single MMF. The output speckle patterns from all MMFs are recorded simultaneously by a large-area camera (with a large number of pixels). Then, they are separately processed in parallel, greatly reducing the complexity of post-processing and enhancing the speed of spectrum reconstruction. Using five 2-meter-long MMFs, dense spectra centered at $\lambda = 1500 \text{ nm}$

with 100 nm bandwidth are recovered with 0.03 nm resolution in snapshot measurements.

Compared to other high-resolution spectroscopy tools such as the scanning Fabry–Pérot etalon or the virtually imaged phase array (VIPA), a notable advantage of the MMF is that its spectral range is not limited by the FSR. This is because fiber fabrication imperfections (random refractive index variation) and external perturbations (fiber bending, twisting) make the probability of a highly multimode fiber producing identical speckle patterns at distinct wavelengths extremely low. A MMF spectrometer, combined with an optical frequency comb source, has been adopted in broadband metrology-grade spectroscopy to resolve individual comb lines.²¹⁶ The wavelength resolution obtained with a 100-m-long MMF is an order of magnitude higher than that of existing dual-comb spectroscopy. Using the MMF spectrometer, 500 comb lines are measured simultaneously and 3500 lines sequentially for direct comb spectroscopy.

The resolving power of a MMF spectrometer can be further improved by increasing the fiber length and/or the differential group delay. However, the speckle patterns are sensitive to environmental changes including mechanical vibration and temperature drift. Recent studies show that a combination of thermal and mechanical stabilization with software correction can enable robust performance of a high-resolution MMF spectrometer.^{212,216} Alternately, the spectral-to-spatial PSF $P(\rho, \phi; \lambda)$ may be calibrated as a function of temperature, and the one matched to the current temperature will be used for spectrum recovery.

Further stabilization is realized with on-chip implementation of the MMF spectrometer. As shown in Fig. 15(a), a silicon multimode waveguide (width = $10 \mu\text{m}$, length = 18 mm) is coiled in an Archimedean spiral (outer radius $250 \mu\text{m}$).²¹⁷ By introducing evanescent coupling of light between adjacent waveguide arms (separated by small air gap), photons will leap forward or backward in time, greatly increasing the temporal spread. Consequently, the spectral resolution is dramatically enhanced [Fig. 15(b)], and such enhancement is non-resonant and broadband. The coupling of waveguide modes, which is detrimental to a MMF spectrometer, improves the resolution by enhancing the evanescent coupling of lower-order modes in adjacent waveguide arms indirectly (converting to higher-order modes with stronger evanescent coupling and then back). The resolving power exceeds 10^5 at the $\lambda \simeq 1500 \text{ nm}$. Like the MMF, the spiral waveguide effectively disperses light at any wavelength as long as the material absorption is negligible and the waveguide remains multimode. Despite the spatial domain is reduced to 1D, a small number of sensors can cover many more spectral channels, if the spectrum is sparse in some domain.²¹⁷ Compressive sensing algorithms are adopted for rapid and accurate reconstruction of various types of sparse spectra [one example given in Fig. 15(c)].

Since the output speckle pattern varies with the launch condition of input light, it is crucial to ensure the consistency between the launch used in PSF calibration and that in spectrum measurement. This is done by coupling signals via a single-mode, polarization-maintaining fiber/waveguide to the multimode fiber/waveguide. To recover a large number of spectral channels N_λ , it is important to excite as many modes as possible at the input. This is realized by using a fiber mode scrambler²¹⁸ or off-set fusion of fibers.²¹⁹

The input launch condition may be switched among multiple choices to increase the number of spectral channels N_λ . On-chip

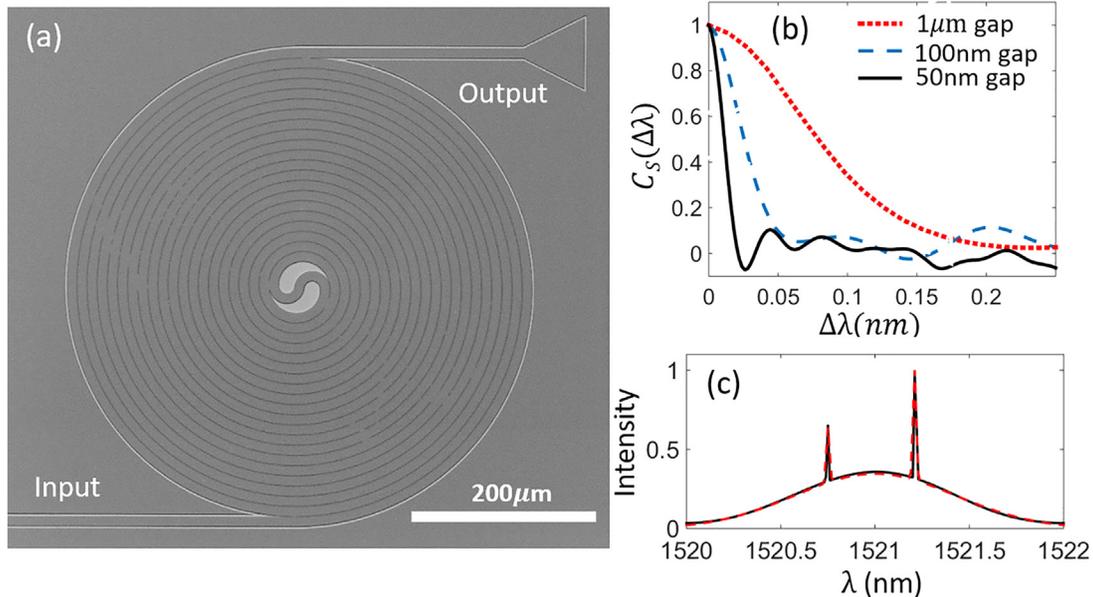


FIG. 15. Spiral waveguide spectrometer in a silicon chip. Reprinted with permission from Redding *et al.*, *Optica* 3, 956 (2016). Copyright 2016 The Optical Society. (a) A multi-mode waveguide of width $10\ \mu\text{m}$ and length $18\ \text{mm}$ is coiled into an interleaved Archimedean spiral structure. (b) Spectral correlation function $C_s(\Delta\lambda)$ measured for three spiral structures with different width of air gaps in between adjacent arms. Narrower air gaps results in stronger evanescent coupling between spiral arms, thus spectral correlation width is smaller and wavelength resolution is better. (c) A reconstructed spectrum has two sharp lines of different amplitude on top of a broad smooth band.

launchers are implemented to vary relative phases and amplitudes of M_w excited modes.²²⁰ With M_w distinct launch conditions, N_λ is increased from M_w to approximately M_w^2 . The space-division multiplexing scheme is also implemented with a multicore fiber²²¹ or an on-chip photonic lantern.²²²

E. Computational spectrometers

The speckle-based spectrometers discussed in Subsections IV A–IV D belong to a general class of computational spectrometers. In addition to spatial speckles, temporal speckles generated by a single-mode fiber (SMF) via Rayleigh backscattering are exploited for a high-precision, broad-range wavemeter.^{223,224} Speckles are also utilized to enhance spectral resolution and dynamic range of prism spectrometers,^{225,226} tapered fiber/waveguide multimode interference spectroscopy,^{227–229} and on-chip Fourier-transform spectrometers.²³⁰

While the speckle spectrometers have fine resolution, broad bandwidth and high throughput, their sensitivity is limited by single-mode collection of signals. Thus, they are most suitable for those applications where single-mode fibers are already used for signal collection, for example, optical wavemeters, telecommunication channel monitors, micro-photoluminescence or micro-Raman spectroscopy, and optical coherence tomography. For volumetric Raman and fluorescence spectroscopy of diffuse sources like tissue and gases, it is essential to use a spectrometer capable of measuring the spectral densities averaged over many spatial modes, in order to improve the SNR. The multimodal spectroscopy is realized with disordered photonic crystals such as 3D opal structures, which can convert spatially incoherent signals with spatially uniform spectral density into spatially non-uniform spectral densities over a detection plane.²³¹

An array of spectral filters has also been used for snapshot spectrum measurement. Compared to narrow bandpass filters, broadband random spectral filters provide more efficient and accurate spectrum recovery.^{232,233} The random transmission spectra are obtained from binary dielectric layers of varying thickness^{234,235} or 2D photonic crystals of different lattice.²³⁶ Since the transmittance of these interference filters is sensitive not only to the input spectrum but also to the angle of incidence, the signals must have a fixed direction of propagation in the spectrum measurement. The spectral filters based on absorption of colloidal quantum dots,²³⁷ which are independent of incident angles, are able to characterize large étendue sources. However, the signal is divided among many filters of different spectra, and the overall throughput is low.

V. SNAPSHOT HYPERSPECTRAL IMAGERS

Since a speckle pattern encodes both spatial and spectral information, it can be used for single-shot hyperspectral imaging. This section describes several schemes of utilizing random spatial-spectral coupling to achieve hyperspectral imaging with single acquisition.

Traditional hyperspectral imagers rely on spatial or spectral scanning, which can be slow and generally require moving parts. Snapshot techniques have been developed to capture the full hyperspectral datacube in a single shot. A common method uses tiled superpixels, each comprised of a grid of spectral filters. While the spectral resolution and/or range increases with the number of spectral filters in one superpixel, the size of a superpixel also increases and the spatial resolution decreases. Moreover, the narrow passbands of spectral filters make the overall light transmission low. To improve the throughput and sensitivity, the absorptive color-filter array is replaced by a transparent diffractive-filter array, each filter generating a wavelength-dependent

diffraction pattern in a camera.^{238,239} However, the short distance between the filter array and the camera limits the spectral resolution. High spectral accuracy can be obtained by replacing the diffractive filters by 2D photonic crystal slabs,²³⁶ but the field of view is limited by a small number of superpixels.

The spectral filter array has also been replaced by a random scattering film, for example, a semiconductor nanowire mat.²⁴⁰ A microlens array focuses light to the nanowire mat, which induces multiple scattering and creates an array of speckle patterns. From these patterns, the position-dependent spectra are recovered. The spatial resolution is given by the microlens spacing, and it is ultimately limited by the diffuse spot size of transmitted light, which scales with the film thickness. For example, a strongly scattering GaP nanowire film is thinner than 2 μm, so the spatial resolution can be potentially high, but the throughput is relatively low. Moreover, the number of speckle grains generated from each focus determines the wavelength range or the number of spectral channels that can be recovered in one measurement.

By resorting to the optical memory effect, multispectral imaging can be realized without a microlens array.²⁴¹ A prototype in Fig. 16(a) consists of a diffuser, an iris and a monochrome camera. As described in Sec. III B, the angular memory effect leads to shift-invariant PSF in the far field. When an object O is illuminated by a single wavelength λ , the far-field speckle intensity pattern is a convolution of the object O_λ and the PSF P_λ , $I_\lambda = O_\lambda * P_\lambda$. The object O_λ can be reconstructed by deconvolution of I_λ with P_λ . Under multi-wavelength illumination, the total intensity pattern is a sum of I_λ :

$$I = \sum_{\lambda} I_{\lambda} = \sum_{\lambda} (O_{\lambda} * P_{\lambda}). \quad (13)$$

Due to random scattering and wave interference, the PSF P_λ decorrelates with wavelength [Fig. 16(b)]. Assuming the PSFs at all illuminating wavelengths are uncorrelated, the deconvolution of I with P_λ is approximately equal to the deconvolution I_λ with P_λ , which gives O_λ [Fig. 16(c)],

$$O_{\lambda} = I_{\lambda} \circledast P_{\lambda} \approx I \circledast P_{\lambda}, \quad (14)$$

where \circledast denotes deconvolution. In essence, each spectral PSF P_λ plays the role of a spectral filter in image reconstruction. Note that the single wavelength λ can be extended to a spectral band. The single speckle image I of an object O contains both spatial and spectral information, which are multiplexed orthogonally via multispectral PSFs P_λ . The deconvolution will de-multiplex and recover the spectral image O_λ [Fig. 16(d)].

One advantage of using random scattering medium for multi-spectral imaging is the flexibility in implementation to utilize the full capacity of a 2D camera.²⁴¹ Instead of being preset at manufacture, the trade-off between spatial and spectral information is up to the analyzer's choices. On one extreme, the spectral information may be limited to a single wavelength or narrow spectral band, and the maximum spatial information is recovered with a maximal number of spatial pixels and dynamic range. On the other extreme, the spatial information is reduced to a single point object, and the highest spectral resolution of the point source is retrieved. Eventually, the number of spatial points in the object and the number of decorrelated spectral bands

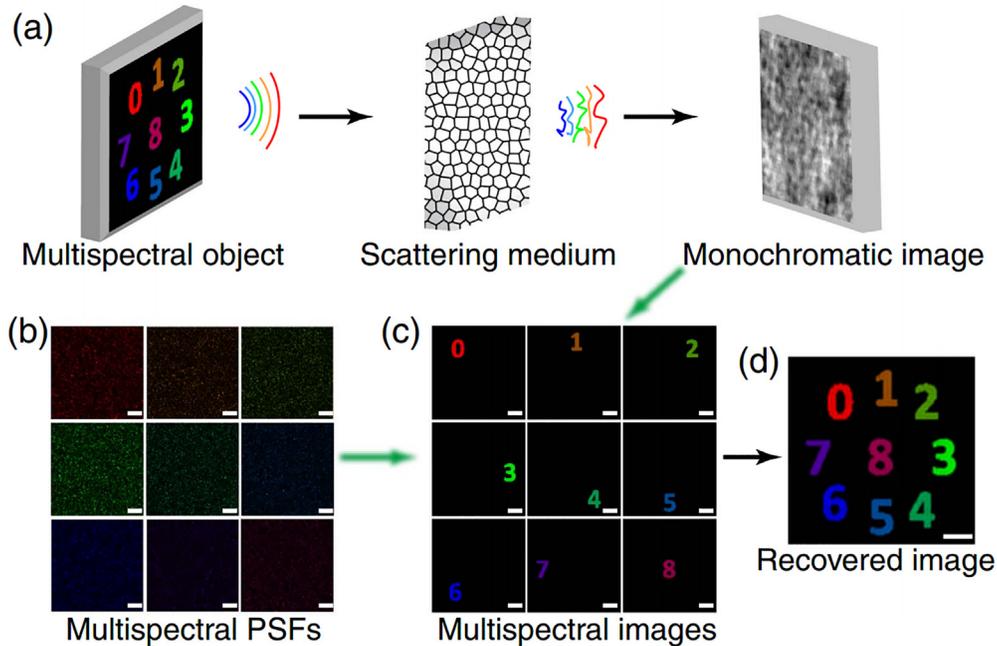


FIG. 16. Speckle-based multispectral imager. Reprinted with permission from Sahoo *et al.*, *Optica* 4, 10 (2017). Copyright 2017 The Optical Society. (a) Schematic of multispectral imaging with a scattering medium and a monochrome camera. Light from a multispectral object propagates through the scattering medium and generates a speckle pattern on the camera. (b) Speckle patterns produced by a point object located at center and illuminated with different spectral bands are recorded as spectral PSFs. (c) Reconstructed spectral images from the monochromatic speckle pattern using corresponding spectral PSFs. (d) A full-spectrum image of the object is created by superimposing of individual spectral images. All scale bars denote 20 pixels in numerical simulation.

determine the intensity contrast of the speckle pattern and therefore the recovery quality of the multispectral images. If a hyperspectral object consists of sparse spectral lines spread over a broad spectral range, a large amount of spatial information can be retrieved with high spectral resolution. One potential issue is the crosstalk caused by residual correlation of PSFs at nearby wavelengths.

Another advantage of the speckle-based multispectral imager is its insensitivity to optical (mis)alignment. There are no moving parts and no focusing optics. Due to the memory effect, a small shift in the optical setup causes only a slight shift of reconstructed multispectral images, and thus, there is no need to recalibrate the multi-spectral PSFs.²⁴¹ Compressive sensing algorithms have been developed to recover spatial and spectral information from snapshot images taken with a monochrome camera.²⁴² The quality of recovery is improved by adding a second camera (regular red-green-blue camera) or using additional scattering medium, after splitting the signal.^{243,244}

Another design of the lensless hyperspectral imager combines a diffuser and a tiled spectral filter array.²⁴⁵ The spectral information at one spatial location is distributed over many superpixels, each containing an array of spectral filters. Therefore, each point in the scene is mapped to a unique pseudo-random pattern on the 2D spectral filter

array, encoding multiplexed spatio-spectral information. By solving a sparsity-constrained inverse problem, the hyperspectral volume is recovered with sub-superpixel resolution. Since the multiplexing effect of the diffuser allows the recovery of a scene from a subset of sensor pixels, the full spatio-spectral cube can be recovered without the loss in resolution that would result from using a non-multiplexing optic such as a lens. The spectral filters are not necessarily contiguous in wavelength; instead, they can be chosen for specific applications. Selecting narrowband spectral filters will lead to high spectral accuracy and discrimination, but at the cost of low light-throughput. As the signal is distributed over many filters, the SNR is further reduced.

To enhance light throughput and spectral resolution, the scattering medium and spectral filters are replaced by a multicore multimode fiber.²⁴⁶ As shown in Fig. 17, 3000 fiber cores provide sub-nanometer wavelength resolution over a broad spectral range. In addition to compressive sensing algorithms, deep learning has been employed for fast and reliable reconstruction of both discrete and continuous spectra from speckle patterns.¹⁹⁸ The artificial neural network is trained with the multispectral datasets numerically constructed from the measured spectral PSFs. Compared to analytical inversion methods and compressive sensing algorithms, the deep learning approach is robust to

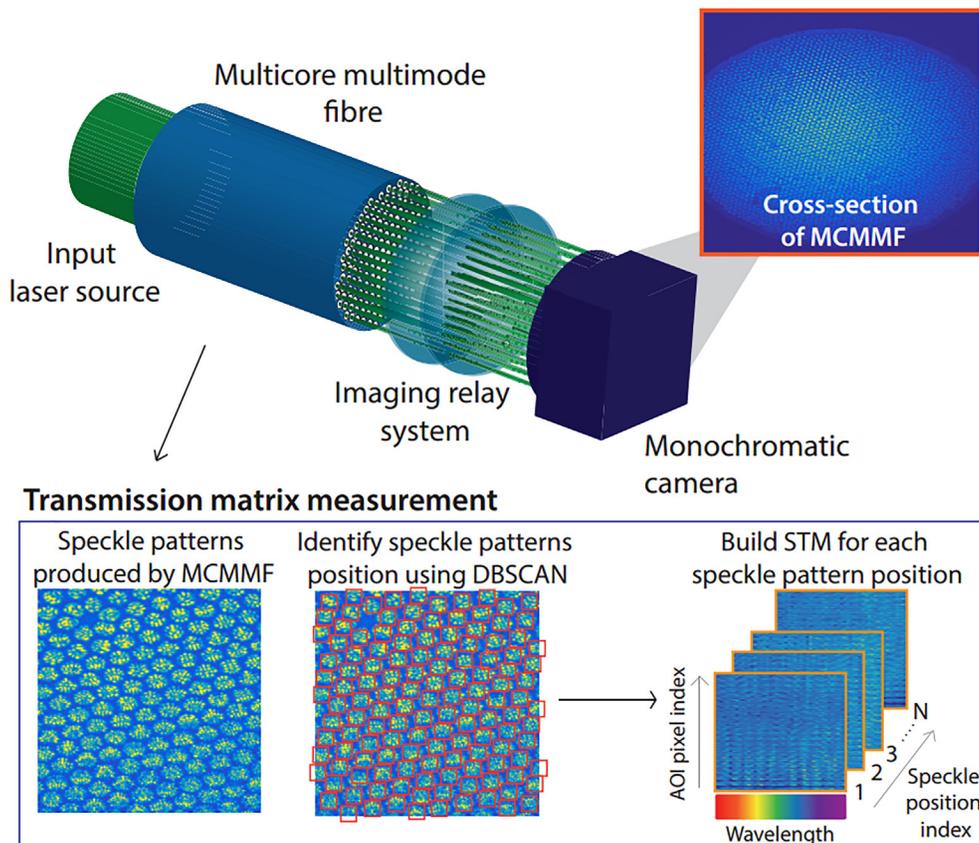


FIG. 17. Hyperspectral imaging with multicore multimode fiber. Reprinted with permission from French *et al.*, *Opt. Express* **26**, 32302 (2018). Copyright 2018 The Optical Society. Light travels through a multicore multimode fiber (MCMMF) and the cross section of the end of the fiber is imaged on to a camera. A clustering algorithm, DBSCAN, detects the coordinates of the speckle patterns produced by each fiber core on the camera. The pattern coordinates are then used to calibrate a spectral intensity transmission matrix (STM) by measuring wavelength-dependent speckle patterns at every core position and storing them in a three-dimensional data cube.

system drift and measurement noise. Although it takes time to train an artificial neural network, once it is done, the reconstruction is fast enough for real-time recovery of hyperspectral information.

VI. SCATTERING POLARIMETERS

The vectorial nature of light plays an indispensable role in light-matter interaction, optical sensing and imaging applications. In Secs. III–V, the polarization states of signals are fixed. In this section, we describe how the vector components of light can be measured using disordered structures. Since multiple scattering of light in complex media encodes spatial, spectral, and polarization information of input signals to output speckle patterns, it is possible to reconstruct spatially resolved (Sec. VIA) and spectrally resolved (Sec. VIB) polarization states from a single image.

A. Spatial polarimetry

When light propagates through a 3D disordered structure or a multimode fiber, it is depolarized (Fig. 18). The change of polarization state is deterministic for a specific configuration of the system and is fully captured in the polarization-resolved transfer matrix for coherent light.²⁴⁷ Without loss of generality, we use the horizontal (H) and vertical (V) linear polarizations as the basis to decompose any coherent polarization state. Equation (3) is generalized to:

$$\begin{bmatrix} \mathbf{E}_{\text{out}}^H \\ \mathbf{E}_{\text{out}}^V \end{bmatrix} = \begin{bmatrix} \mathbf{M}_{HH} & \mathbf{M}_{HV} \\ \mathbf{M}_{VH} & \mathbf{M}_{VV} \end{bmatrix} \cdot \begin{bmatrix} \mathbf{E}_{\text{in}}^H(\mathbf{r}) \\ \mathbf{E}_{\text{in}}^V(\mathbf{r}) \end{bmatrix}. \quad (15)$$

$\mathbf{E}_{\text{in}}^H(\mathbf{r})$ and $\mathbf{E}_{\text{in}}^V(\mathbf{r})$ represent horizontal and vertical components of the input field profile, and $\mathbf{E}_{\text{out}}^H(\mathbf{r})$ and $\mathbf{E}_{\text{out}}^V(\mathbf{r})$ of the output. The polarization-resolved transfer matrix contains four submatrices \mathbf{M}_{HH} , \mathbf{M}_{HV} , \mathbf{M}_{VH} , and \mathbf{M}_{VV} . \mathbf{M}_{HV} and \mathbf{M}_{VH} account for polarization conversion by optical scattering. Once the full matrix is calibrated, the spatially varying polarization state of an input signal can be recovered from polarization-resolved measurement of the output field profile.²⁴⁸

Equation (15) holds for coherent polarization states. A more general description of polarization that is valid for both coherent and incoherent states is the Stokes vector \mathbf{S} . It contains four independent parameters (S_1, S_2, S_3, S_4). If the polarization state of a signal beam is

spatially invariant, the Stokes vector can be reconstructed from four measurements of spatial intensity correlations of speckle patterns generated by a disordered structure.^{249,250} First, four reference speckle patterns, produced by a scattering medium for four known polarization states of the input light, are recorded. For example, the four reference polarization states are three linear polarizations and one right-handed circularly polarization (+). The first three linear polarizations are oriented to the x -axis (0°), the y -axis (90°), and 45° , respectively. The corresponding speckle patterns transmitted through or reflected from a scattering medium are R_x, R_y, R_{xy} , and R_+ . Then, a signal of unknown polarization but with identical spatial waveform to the reference light generates a speckle pattern R_s . It is cross-correlated with four reference speckle patterns R_i , where $i = x, y, xy, +$. The normalized cross-correlation coefficients $C_i = \langle R_s | R_i \rangle$ give the Stokes parameters of the signal,

$$\begin{aligned} S_1 &= C_x + C_y, \\ S_2 &= C_x - C_y, \\ S_3 &= 2C_{xy} - (C_x + C_y), \\ S_4 &= 2C_+ - (C_x + C_y). \end{aligned} \quad (16)$$

Now we consider a signal with spatially varying polarization, namely, the Stokes vector \mathbf{S}_{in} changes with position \mathbf{r} . It has been shown that the output speckle intensity pattern is linearly related to the input Stokes parameters, as long as light scattering is linear.²⁵¹ The output intensity pattern $\mathbf{I}_{\text{out}}(\mathbf{r})$ is expressed as

$$\mathbf{I}_{\text{out}}(\mathbf{r}) = \tilde{\mathbf{M}}_S \cdot \mathbf{S}_{\text{in}}(\mathbf{r}). \quad (17)$$

$\mathbf{S}_{\text{in}}(\mathbf{r})$ is a vector with $4N_{\text{in}}$ elements, describing the polarization states of input light at N_{in} spatial positions. $\mathbf{I}_{\text{out}}(\mathbf{r})$ is a vector with N_{out} elements, denoting the output intensities at N_{out} positions. The transfer matrix $\tilde{\mathbf{M}}_S$ describes a linear mapping from $\mathbf{S}_{\text{in}}(\mathbf{r})$ to $\mathbf{I}_{\text{out}}(\mathbf{r})$. Once $\tilde{\mathbf{M}}_S$ is calibrated or learned, the Stokes parameters can be recovered from the spatial intensity pattern recorded by a camera.

Compared to conventional polarimeters, the scattering polarimeter enables a single-shot measurement of all Stokes parameters. For a signal beam with spatially invariant polarization, \mathbf{S}_{in} has only four parameters, which can be recovered from the speckle intensities at

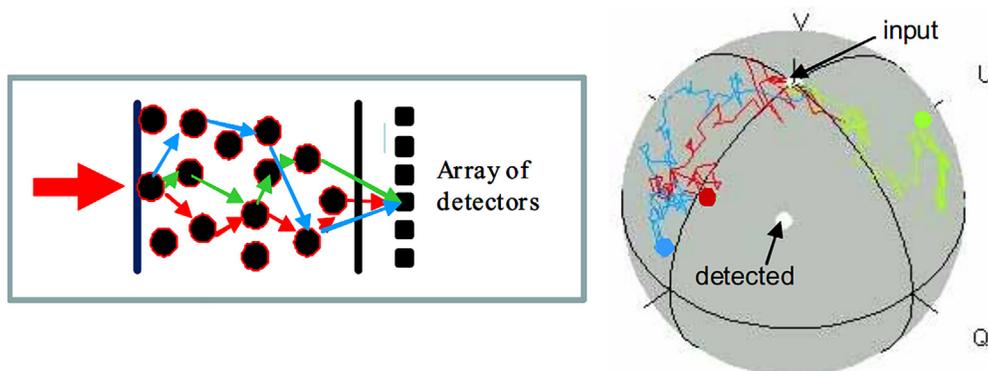


FIG. 18. Depolarization by multiple scattering. Reprinted with permission from Kohlgraf-Owens and Dogariu, *Opt. Express* **16**, 13225 (2008). Copyright 2008 The Optical Society. Light incident onto a disordered system undergoes multiple scattering, which changes its polarization state, as shown by the Poincaré sphere on the right. With a static scattering structure, the deterministic relation between the input and output vector fields allows retrieval of the input polarization state from the output intensity pattern.

four spatial positions. Once the output speckle pattern is recorded in a single shot, the intensities at additional positions may be used to enhance the accuracy of polarization recovery. If the input signals in N_{in} spatial channels have distinct polarization states, a minimum of $N_{\text{out}} = 4N_{\text{in}}$ intensities are extracted from the output speckle pattern to determine N_{in} input polarization states.²⁴⁸ If there is prior information about the signal polarization state or the signal is spatially sparse, the number of output intensities needed for polarization recovery is reduced by using compressive sensing algorithms. This method is also applied to simultaneous measurement of polarization states of multiple laser beams that are mutually incoherent.²⁵¹ It has been shown that the polarization rotation of a signal beam can be tracked from the temporal change of the speckle pattern.^{249,252}

B. Spectral polarimetry

Subsection VI A considers monochromatic light. If the input light contains multiple wavelengths, the output speckle pattern encodes spatial, spectral, and polarization information. More specifically, Eq. (17) can be generalized to

$$\mathbf{I}_{\text{out}}(\mathbf{r}) = \int \tilde{\mathbf{M}}_S(\lambda) \cdot \mathbf{S}_{\text{in}}(\mathbf{r}; \lambda) d\lambda. \quad (18)$$

In principle, the spatially and spectrally resolved Stokes vector $\mathbf{S}_{\text{in}}(\mathbf{r}; \lambda)$ can be recovered from a single speckle pattern $\mathbf{I}_{\text{out}}(\mathbf{r})$, but the finite number of speckle grains will limit the total amount of information in space, spectrum, and polarization that can be retrieved from one measurement.

If the signal is spatially homogeneous or one spatial mode is probed, only its spectrum and polarization need to be recovered. The polarization state may vary with wavelength; namely, each wavelength has distinct polarization. To recover $\mathbf{S}_{\text{in}}(\lambda)$ from $\mathbf{I}_{\text{out}}(\mathbf{r})$, the transfer matrix $\tilde{\mathbf{M}}_S(\lambda)$ must be calibrated first. One implementation of the spectral polarimeter is covering one end of an imaging fiber bundle with a thin layer of $0.5 \mu\text{m}$ silica spheres.²⁵³ Because the spheres are located randomly with respect to the fiber core centers, different cores have widely varying responses, both spectrally and polarimetrically. The other end of the fiber bundle is imaged onto a CCD camera. From the speckle patterns, signals with spectrally varying polarization states are recovered.²⁵³ However, the spectral resolution is modest, because the scattering layer is kept thin to avoid low throughput.

The spectral resolution can be boosted by multiple scattering of light. Let us consider the 2D diffusive structure in the chip-scale spectrometer (Fig. 13). Since the transverse-electric (TE) and transverse-magnetic (TM) waves have slightly different effective indices of refraction in a thin silicon layer, the scattering cross section of a single air hole differs slightly for the two polarizations. Such difference is accumulated by scattering subsequently with multiple holes, leading to distinct intensity patterns at the sensor array. Their orthogonal polarizations result in an intensity sum at each sensor, and thus, the total intensity distribution is given by

$$I_{\text{det}}(x) = \int \left[P_H(x; \lambda) I_{\text{sig}}^{(H)}(\lambda) + P_V(x; \lambda) I_{\text{sig}}^{(V)}(\lambda) \right] d\lambda. \quad (19)$$

From $I_{\text{det}}(x)$, the input spectra for TE polarization $I_{\text{sig}}^{(H)}(\lambda)$ and TM polarization $I_{\text{sig}}^{(V)}(\lambda)$ can be reconstructed, because the spectral PSFs for the two polarizations $P_H(x; \lambda)$ and $P_V(x; \lambda)$ are notably different.

Equation (19) assumes the polarization mixing by in-plane scattering is negligible. If this is not the case, the input TE wave may be converted to a TM wave and interfere with the original TM wave at the same wavelength. Then, the intensity sum must be replaced by a field sum. However, if the input TE and TM waves are mutually incoherent at all wavelengths, the intensity sum will remain valid even in the presence of polarization mixing. Hence, the spectra for two polarizations can still be recovered using Eq. (19).

VII. TEMPORAL MEASUREMENT

Now we shift to the time domain and show how time-integrated speckle patterns from multimode optical fibers/waveguides are employed to retrieve temporal information at both radio frequency and optical frequency. In Sec. VII A, radio frequency (RF) receivers based on optical speckle detection break the Nyquist sampling limit by employing compressive (compressed) sensing techniques. Section VII B presents two schemes for single-shot full-field recovery of ultra-short optical pulses, one utilizing spatiotemporal speckle fields generated by a multimode fiber for parallel ghost imaging, the other based on nonlinear speckle measurement and deep learning.

A. Compressive radio-frequency receivers

Nyquist rate sampling of Gigahertz-band radio frequency (RF) signals rapidly generates huge amounts of data. To address this general issue, compressive sensing (CS) techniques are developed for sparse signals and images. Electronic CS systems suffer timing jitter and amplitude noise. Although microwave photonic CS systems have equivalent issues, in many cases, the distortions are static or lower in frequency and amenable to calibration. Previously, pseudo-random bit sequences have been created to modulate the optical carriers for compressive sensing. Recently, optical speckle patterns, generated by multimode fibers or waveguides, are employed for sparse RF signal recovery.^{218,254,255}

Figure 19 is a schematic showing a multimode waveguide/fiber replacing a 2D SLM in generating pseudo-random bit sequences in a modulated wideband converter.²¹⁸ Femtosecond pulses from a mode-locked laser (MLL) are launched into a dispersion-compensating fiber (DCF), which stretches the pulse to the inter-pulse time. Then, the optically chirped pulses pass through a Mach-Zehnder modulator (MZM) that imprints the RF signal on the optical intensity and subsequently enter a multimode waveguide/fiber. The transmitted signals are spatially split at the output of the guide and directed to an array of photodiodes. The integration times of the photodiodes are matched to the period of mode-locked pulses, and the electrical signals from the photodiode array are digitized by an array of analog-to-digital converters (ADCs) clocked to the pulse repetition rate. An optional fiber mode scrambler is placed near the input end of the fiber to fully excite the guided modes. The time-wavelength mapping is depicted by the rainbow-colored pulse icons. The output speckle pattern from the multimode waveguide varies with wavelength, and hence with time. The optical spectrum recovered from the speckle pattern provides temporal variation of the RF signal through the time-wavelength mapping. CS algorithms are employed to recover different types of sparse signals, for example, sparse in time, in frequency, or after the Harr wavelet transform.²¹⁸

Instead of mapping from space to wavelength and then to time, it is possible to combine them for a direct mapping from space to time

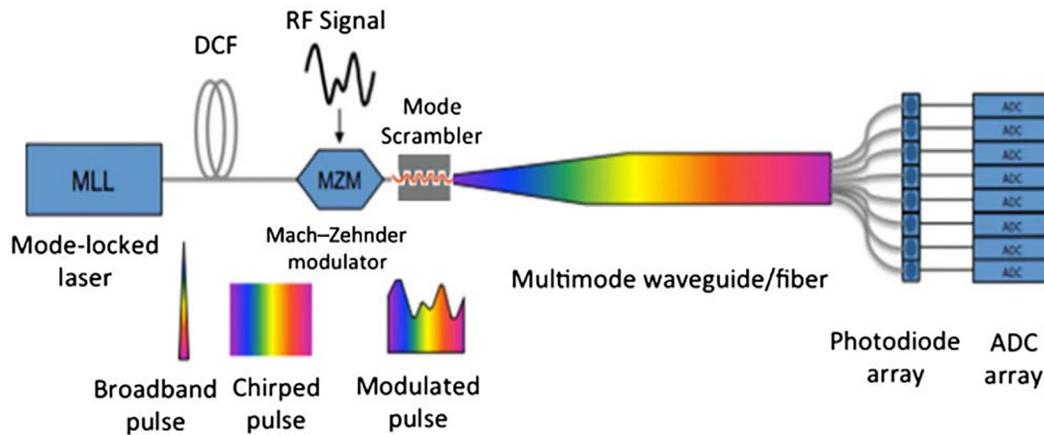


FIG. 19. Compressive sensing of RF signals. Reprinted with permission from Valley *et al.*, *Opt. Lett.* **41**, 11 (2016). Copyright 2016 The Optical Society. Schematic of RF signal recovery from optical speckle measurement. An broadband optical pulses from a mode-locked laser (MLL) are stretched by a dispersion compensating fiber (DCF), and the RF signals are applied to the chirped pulse in a Mach-Zehnder modulator (MZM), and then, the modulated pulses are sent through a multimode waveguide/fiber, and the transmitted speckle patterns are detected by a photodiode array.

or to RF. In addition to the RF signal amplitude, its relative phase (with respect to the optical pulse train from the mode-locked laser) can be recovered from the speckle measurement. The mapping matrix has two columns for each RF tone, which are referred to as in-phase and quadrature components. Three methods have been explored for calibration: the first one estimates the two columns from measurements with pairs of pulses, the second method fits the data as a function of the relative RF phase, and the third one is based on singular value decomposition (SVD) of the calibration matrix.²⁵⁴ Finally, a penalized l_1 norm method recovers the amplitude, phase, and frequency of sparse RF signals. Using a 5-m-long MMF (0.22 NA step-index, 105- μm core), RF signals with one tone or two tones in the 2–19 GHz band are reconstructed with 100 MHz resolution in a single 4.5-ns pulse.

To reduce the device footprint, the MMF is replaced by an 11-cm-long multimode waveguide (96 μm wide and 220 nm thick), which is integrated with a multi-port splitter and a grating coupler array in a photonic circuit.²⁵⁵ The planar waveguide is wrapped in a spiral geometry and produces random projections for CS via optical speckle. A precise analog signal routing is supported by two integrated structures, waveguide bus trombone flare and matched 90° bus bend, in the silicon chip. 16 RF channels, each with an effective sampling rate of 35 MSps (mega samples per second), are able to recover RF signals across a 2 GHz bandwidth from 2.5 to 4.5 GHz. Compared with direct Nyquist sampling, which requires 4 GSps, the CS requires $4000/(35 \times 16) = 7$ times fewer recorded samples and a maximum sampling rate that is $4000/35 = 114$ times smaller.²⁵⁵ Sampling well below the Nyquist limit reduces the need for data storage, shortens data-payload transmission time, and reduces the overall receiver size, weight, and power.

B. Single-shot full-field measurement of optical pulses

Full-field (both amplitude and phase) characterization of ultra-short optical pulses with femtosecond to attosecond pulse duration is crucial to ultrafast science. Existing sensors are not fast enough to

directly resolve such short pulses, and the pulses are recovered indirectly, often through algorithmic methods. Various schemes have been developed for multi-shot measurements, which require trains of identical pulses. However, in many cases the probed pulses are not reproducible, prompting the development of single-shot characterization methods.

The single-shot measurement is more challenging for several reasons. First, a trade-off between the temporal range Δt and resolution δt limits the time-bandwidth product $\Delta t/\delta t$, where $1/\delta t$ is proportional to the spectral bandwidth. Second, the single-shot measurement is highly sensitive to noise, as there is no averaging over multiple pulses and the power of incoming signal is always limited. Third, a full-field characterization requires recovering the amplitude $A(t)$ and phase $\theta(t)$ simultaneously, and both may evolve rapidly in time t .

A Fourier transform of the temporal field $E(t) = A(t)e^{i\theta(t)}$ gives the spectral field $E(\omega) \equiv \mathcal{F}[E(t)] = A(\omega)e^{i\theta(\omega)}$. Simultaneous reconstruction of spectral amplitude $A(\omega)$ and phase $\theta(\omega)$ will recover $E(\omega)$ and $E(t)$. As shown in Sec. IV, the power spectrum $I(\omega) = |E(\omega)|^2 = [A(\omega)]^2$ can be reconstructed from a time-integrated intensity measurement of optical speckle pattern generated by a random scattering medium or a multimode fiber/waveguide. However, such speckle pattern does not contain any information of spectral phase, thus preventing complete pulse recovery.

Lately, two methods are developed for single-shot full-field measurement of optical pulses using (i) spatiotemporal speckles and (ii) nonlinear speckles. This subsection will introduce these methods. While method (i) employs a reference pulse, method (ii) is reference-free or self-referenced.

1. Parallel temporal ghost-imaging

Figure 20(a) illustrates the single-shot full-field measurement using spatiotemporal speckle pattern out of a multimode fiber (MMF).²⁵⁶ A linearly polarized laser pulse with known field $f(t)$ is split into two arms of a Mach-Zehnder interferometer. In one arm, the pulse is launched into a multimode fiber (MMF) to create a

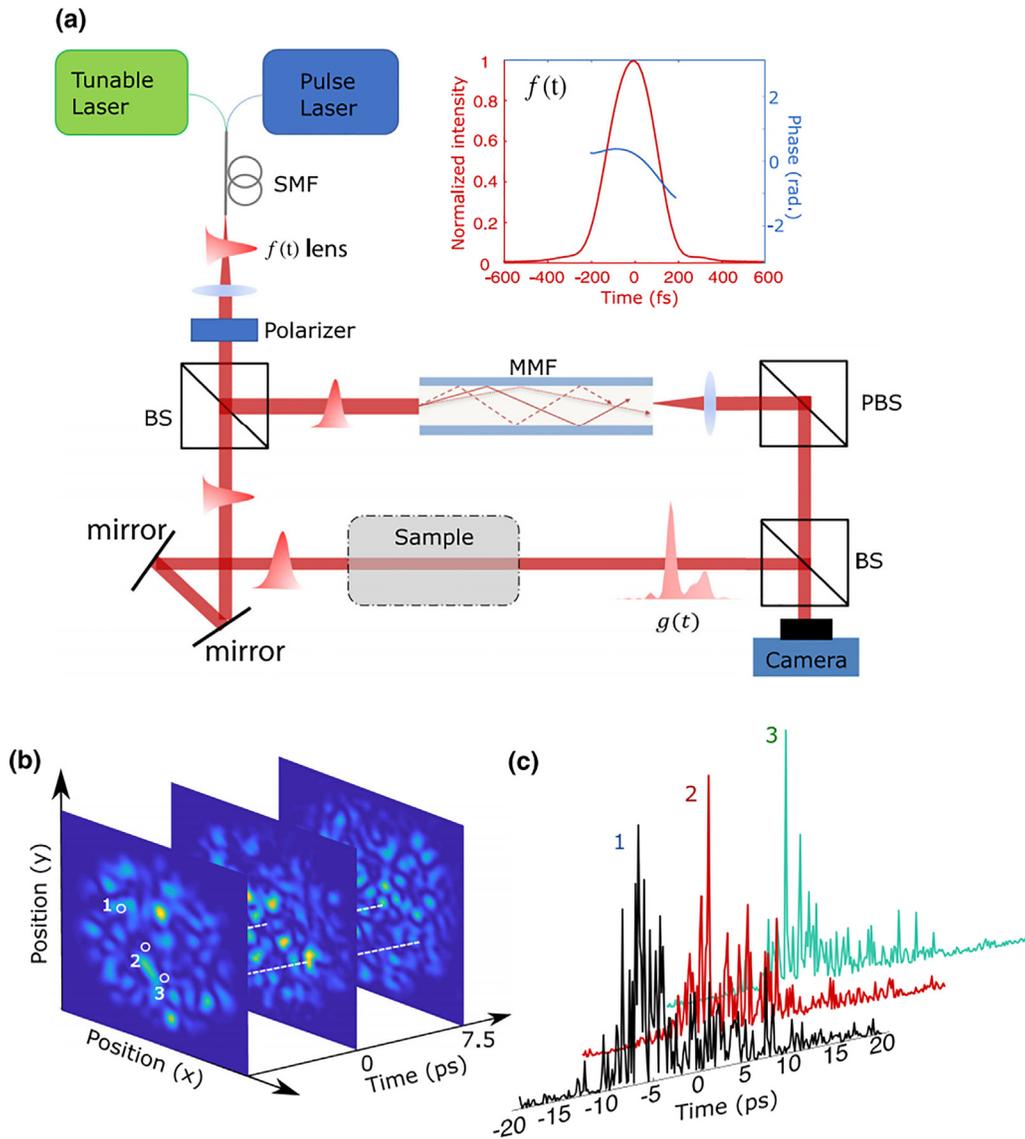


FIG. 20. Single-shot pulse characterization using spatiotemporal speckles. Reprinted with permission from Xiong *et al.*, *Opt. Lett.* **45**, 2462 (2020) Copyright 2020 The Optical Society. (a) Schematic of an interferometric setup for calibration of spatiotemporal speckle field generated by a reference pulse through a multimode fiber (MMF). Its interference with a signal (transmitted pulse of a sample) at a slow camera enables full field recovery of the signal. Inset: intensity (red solid line) and phase (blue solid line) of the reference pulse launched into the MMF. (b) Spatial field amplitude distribution of a reference pulse transmitted through the MMF evolves with time. (c) Transmitted field amplitudes at different spatial positions of the fiber output exhibit distinct temporal fluctuations.

spatiotemporal speckle field $E_s(\mathbf{r}, t)$ in transmission. In the other arm, the pulse interacts with a sample, and the transmitted/reflected field $g(t)$ interferes with $E_s(\mathbf{r}, t)$. The time-integrated intensity pattern $I_p(\mathbf{r}) = \int |E_s(\mathbf{r}, t) + g(t)|^2 dt$ is recorded by a slow camera. By applying a Hilbert filter in the Fourier domain of $I_p(\mathbf{r})$, the interference term $I_q(\mathbf{r}) = \int dt [E(\mathbf{r}, t) g^*(t) + E^*(\mathbf{r}, t) g(t)]$ is extracted.

In the frequency domain, $E_s(\mathbf{r}, \omega) = \mathcal{F}[E_s(\mathbf{r}, t)] = T(\mathbf{r}, \omega) F(\omega)$, where $T(\mathbf{r}, \omega)$ is the frequency-resolved field transmission matrix of the MMF, and $F(\omega) = \mathcal{F}[f(t)]$. The interference term can be expressed in the frequency domain as

$$I_q(\mathbf{r}) = \begin{bmatrix} T(\mathbf{r}, \omega) f(\omega) & T^*(\mathbf{r}, \omega) f^*(\omega) \end{bmatrix} \begin{bmatrix} g^*(\omega) \\ g(\omega) \end{bmatrix}, \quad (20)$$

where $G(\omega) = \mathcal{F}[g(t)]$. Once $T(\mathbf{r}, \omega)$ is calibrated and $F(\omega)$ is known, $G(\omega)$ can be retrieved from $I_q(\mathbf{r})$, and an inverse Fourier transform gives $g(t)$.

The temporal range Δt of the single-shot measurement is set by the temporal length of $E_s(\mathbf{r}, t)$, which is inversely proportional to the spectral correlation width of the MMF. A fiber with longer length and/or stronger modal dispersion has a faster spectral decorrelation and

can cover a longer time window. The temporal resolution δt is equal to the temporal speckle size, which is given by the inverse of the spectral bandwidth of the reference pulse. A reference pulse of broader bandwidth (not necessarily transform-limited in time) provides higher temporal resolution. Therefore, the temporal range and resolution can be tuned separately by varying the parameters of the fiber and the reference pulse. Experimentally, single-shot full-field measurement with a 1.8-m-long MMF (105 μm core diameter, 0.22 NA) provides 230 fs temporal resolution over 35 ps window, and the time-bandwidth product is 152.²⁵⁶

The time-bandwidth product reflects the number of independent temporal channels that are measured simultaneously. Its upper bound is given by the number of uncorrelated time traces generated by the MMF, which is equal to the number of guided modes in the fiber. The time-bandwidth product for a MMF with a large core and a high NA may well exceed 1000, and a further increase is possible with a bundle of MMFs.²¹⁵

This single-shot measurement scheme is equivalent to parallel ghost imaging in time.²⁵⁷ While the conventional ghost imaging relies on sequential generation of different temporal waveforms for sampling, the MMF simultaneously creates many distinct time traces in different spatial channels to sample the signal [Fig. 20(c)]. The complex yet deterministic spatiotemporal speckle field enables parallel sampling in a single shot for a full-field recovery, eliminating the requirement for repetitive signals.

The spatiotemporal coupling of broadband light in a MMF has also been employed for axial reflectivity profiling.²⁵⁸ The closely spaced yet distinct propagation constants of various spatiotemporal modes in a MMF yield a set of spatially distributed encoding functions that can be used for depth referencing. A signal that is delayed by reflection at a specific sample depth only interferes with the path length-matched encoding function [Fig. 20(b)] and creates a distinct speckle pattern that is unique to this depth. An arbitrary sample reflectivity profile produces a linear superposition of the associated speckle patterns. By calibrating the random encoding functions, the 1D sample depth profile is reconstructed from a single recording of the interference pattern without the need for any mechanical or optical scanning. Such configuration can be considered as spatially multiplexed low-coherence interferometry and is a parallel implementation of ghost optical coherence tomography.²⁵⁹ Experimentally, axial depth profiling is demonstrated with bandwidth-limited resolution of 13.4 μm over a range of 13.4 mm.²⁵⁸ By varying the MMF length, the depth range is scaled from several millimeters to well beyond one centimeter, relaxing the challenging hardware requirements of achieving similar performance with conventional spectrometer-based coherence gating.

2. Nonlinear speckle and deep learning

The method described in Subsection VII B 1 relies on a known optical pulse that is mutually coherent with the unknown signal. In this subsection, a reference-free time-integrated measurement scheme will be introduced to enable stand-alone single-shot characterization of ultrafast pulses.

The key for full-field recovery is retrieving the spectral phase $\theta(\omega)$, as the spectral amplitude $A(\omega)$ is already reconstructed from the linear speckle pattern. Measuring the relative phase of different spectral components in a pulse requires these components to interfere,

but distinct frequencies do not interfere in a linear, time-integrated detection. To retrieve the spectral phase without any reference, a nonlinear material is placed behind a MMF to create a speckle pattern via two-photon absorption or sum-frequency generation.^{260,261}

As illustrated in Fig. 21(a), the propagation of a signal pulse in the MMF remains linear, so that the transmitted light is related to an incident signal by the field transmission matrix: $E_t(\mathbf{r}, t) = \mathcal{F}^{-1}[T(\mathbf{r}, \omega) A(\omega)]$, where \mathcal{F}^{-1} denotes the inverse Fourier transform. The time-integrated linear speckle pattern $I_{1p}(\mathbf{r}) = \int |E_t(\mathbf{r}, t)|^2 dt = \int |T(\mathbf{r}, \omega)|^2 |A(\omega)|^2 d\omega$ encodes only the spectral amplitude $A(\omega)$ of an input signal. The time-integrated nonlinear speckle pattern $I_{2p}(\mathbf{r}) = \int |E_t(\mathbf{r}, t)|^4 dt$ can be expressed as

$$I_{2p}(\mathbf{r}) = \iiint d\omega_1 d\omega_2 d\omega_3 |T(\mathbf{r}, \omega_1)| |A(\omega_1)| |T(\mathbf{r}, \omega_2)| |A(\omega_2)| \\ \times |T(\mathbf{r}, \omega_3)| |A(\omega_3)| |T(\mathbf{r}, \omega_1 - \omega_2 + \omega_3)| |A(\omega_1 - \omega_2 + \omega_3)| \\ \times e^{i[\theta(\omega_1) - \theta(\omega_2) + \theta(\omega_3) - \theta(\omega_1 - \omega_2 + \omega_3)]} \\ \times e^{i[\theta_{\text{TM}}(\mathbf{r}, \omega_1) - \theta_{\text{TM}}(\mathbf{r}, \omega_2) + \theta_{\text{TM}}(\mathbf{r}, \omega_3) - \theta_{\text{TM}}(\mathbf{r}, \omega_1 - \omega_2 + \omega_3)]}, \quad (21)$$

where $\theta_{\text{TM}}(\mathbf{r}, \omega)$ is the phase of $T(\mathbf{r}, \omega)$. $I_{2p}(\mathbf{r})$ encodes the spectral phase $\theta(\omega)$ of the signal, because different spectral components interfere in the nonlinear optical process. Moreover, the complex interference eliminates ambiguity in the sign of spectral phase, allowing the direction of time to be recovered [Figs. 21(b) and 21(c)]. This is advantageous over other self-referenced nonlinear techniques that cannot distinguish the direction of time.²⁶²

In practice, retrieving the input spectral phase $\theta(\omega)$ from the nonlinear speckle intensity $I_{2p}(\mathbf{r})$ is highly non-trivial, because the inverse mapping from $I_{2p}(\mathbf{r})$ to $\theta(\omega)$ is complicated. Conventional phase retrieval algorithms are sensitive to noise in the nonlinear snapshot measurement and thus cannot provide a reliable recovery. A deep neural network is employed to learn the nonlinear mapping from $I_{2p}(\mathbf{r})$ to $\theta(\omega)$.²⁶⁰ Once the field transmission matrix $T(\mathbf{r}, \omega)$ of the fiber is calibrated, it is straightforward to calculate the nonlinear speckle pattern for any input pulses using Eq. (21). A large amount of data are numerically synthesized to train a convolutional neural network. Furthermore, deep learning is combined with compressive sensing by representing the spectral phase in a sparse basis to dramatically reduce the number of parameters that the neural network predicts. Measurement noise and fiber fluctuation are incorporated to the training data, so that the trained network is robust and outperforms classical algorithms.

Since the nonlinear speckle pattern encodes both amplitude and phase information, it may be used to recover $A(\omega)$ and $\theta(\omega)$ simultaneously, eliminating the linear speckle measurement. Numerically, a deep neural network is trained for pulse amplitude and phase recovery.²⁶¹ This technique is shown to be robust to noise and inaccuracy in system parameters, and capable of reconstructing ultrashort pulses at low SNR. It mitigates the need for iterative optimization, which is usually slow and hampered by the presence of noise. Therefore, the deep learning method is advantageous for real time probing of ultrafast processes under noisy conditions.

The speckle-based pulse characterization scheme can be tuned to measure optical pulses of varying length. The temporal range of measurement is determined by the spectral decorrelation of the MMF, and the temporal resolution depends on the spectral bandwidth over which the field transmission matrix is calibrated. Experimentally, a 1.3-m-

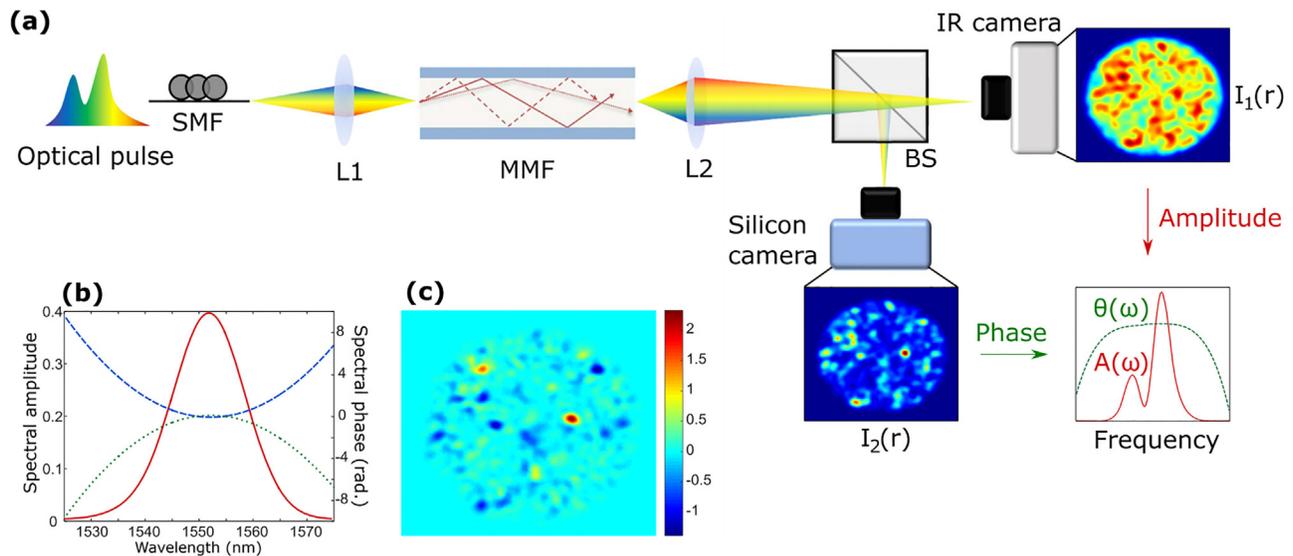


FIG. 21. Full-field recovery with linear and nonlinear speckles. Reproduced with permission from Xiong *et al.*, APL Photonics **5**, 9 (2020). Copyright 2020 AIP Publishing LLC. (a) Schematic of experimental realization. An optical pulse at $\lambda = 1550$ nm is delivered via a single-mode fiber (SMF) to a multimode fiber (MMF). At the MMF output, time-integrated linear speckle pattern $I_1(\mathbf{r})$ is recorded by an IR camera via one-photon absorption, and nonlinear speckle pattern $I_2(\mathbf{r})$ recorded by a silicon camera via two-photon absorption. The spectral amplitude $A(\omega)$ and phase $\theta(\omega)$ of the input pulse are recovered from $I_1(\mathbf{r})$ and $I_2(\mathbf{r})$, respectively. (b) An optical pulse has spectral amplitude $A(\omega)$ (red solid line) and phase $\theta(\omega)$ (blue dashed line). The sign of its phase flipped to $-\theta(\omega)$ (green dotted line), which corresponds to temporal inversion with phase conjugation. (c) Difference in $I_2(\mathbf{r})$ between two pulses with opposite spectral phases in (b) indicates the sign of spectral phase can be recovered from the nonlinear speckle pattern.

long step-index fiber with 105 μm core and 0.22 NA is calibrated over a wavelength range of 1525–1575 nm, and provides a temporal resolution of 160 fs over a time window of 30 ps. The resolution can be further increased by calibrating the MMF over a larger bandwidth, and the temporal range can be extended by using a longer fiber with faster spectral decorrelation. Finally, the MMF may be replaced by a random scattering medium or an on-chip multimode waveguide.

VIII. RANDOM LASERS

Next, we switch to disordered systems that possess optical gain and nonlinearity. In Sec. VIII A, we introduce random lasers and illustrate their distinction from conventional lasers. The applications of random lasers to spatial coherence engineering and speckle-free imaging are covered in Secs. VIII B and VIII C. In analog to super-resolution microscopy, super-resolution spectroscopy is achieved with a random laser in Sec. VIII. Section VIII E presents the random fiber lasers based on stimulated Raman scattering, which produce high-power with high efficiency and exhibit nearly octave wavelength tuning. Section VIII F shows that structural disorder can suppress temporal instability in a semiconductor laser.

A. Introduction of random laser

The essential ingredients of a laser are a gain material that is optically or electrically pumped to amplify light through stimulated emission, and a cavity that increases the dwell time or path length of light in the gain medium to enhance amplification. Although most lasers produce emission with high spatial and temporal coherence, the first-order coherence is not exclusive to lasers.²⁶³ What distinguishes a laser

from a thermal light source is the second-order coherence that results from gain saturation.

Unlike conventional lasers relying on mirrors or periodic structures to trap light, a random laser utilizes multiple scattering in a disordered gain medium for optical confinement and feedback.^{264–266} It has been implemented in many material systems, including powders,²⁶⁷ colloids,²⁶⁸ biological tissues,²⁶⁹ polycrystalline films,²⁷⁰ polymers,²⁷¹ optical fibers,²⁷² and cold atomic vapors.²⁷³ The lasing frequencies range from ultraviolet²⁷⁴ and visible²⁷⁵ to infrared²⁷⁶ and Terahertz.²⁷⁷ This section will cover some applications of random lasers.

B. Spatial coherence engineering

Despite high radiance, high efficiencies, and good spectral control, conventional lasers have not been widely used for illumination in full-field imaging and display applications because of coherent imaging artifacts. Such artifacts originate from the interference of scattered or diffracted waves during image formation, and the resulting intensity modulations appear as additional features that are not present in the object, thereby corrupting the image. The most common manifestation of coherent artifacts is speckle noise, which occurs when a rough object or scattering environment introduces random phase delays among mutually coherent photons that interfere at the detector. To avoid speckle, thermal light sources and light-emitting diodes (LEDs) are commonly used for illumination in most parallel imaging and projection applications, despite having lower power per mode, poorer collection efficiency, and less spectral control than lasers. The limitation of source brightness is particularly pronounced in applications requiring high-speed imaging or imaging with absorbing or scattering background.

For parallel imaging and projection applications, the ideal illumination source will combine the high brightness of a laser and the low spatial coherence of a lamp. The common approach to achieve this combination is reducing the effective spatial coherence of a traditional laser using a time-varying scattering system such as a moving diffuser²⁷⁸ or a colloidal solution.²⁷⁹ Many speckle patterns are generated sequentially and summed to reduce the intensity contrast C_t to $1/\sqrt{N_r}$, where N_r is the number of uncorrelated speckle patterns in the sum. To lower the speckle contrast below the level of human perception $C_t < 3\%$, about 1000 different speckle patterns are needed for averaging, and it takes time to create them in series, which mitigates the advantage of using bright sources like lasers for high-speed imaging applications. Instead of reducing the spatial coherence with moving scatterers outside the laser cavity, incorporation of (static) scatterers in a laser cavity will directly generate emission with low spatial coherence.

Once numerous scattering particles are added to a gain material, the spontaneously emitted photons will be scattered many times and undergo a “random walk.”²⁸⁰ Multiple scattering increases the path length of photons in the gain medium, enhancing the stimulated emission of photons.²⁸¹ Furthermore, the scattered photons may return to spatial positions they have visited before, providing feedback for lasing oscillation.²⁸² Most random lasers operate in the highly multimode regime. Individual lasing modes, formed by interference of scattered waves, have distinct frequencies and spatial structures.²⁸³ If the frequency spacing between neighboring lasing modes $\delta\omega$ exceeds their linewidth, they become mutually incoherent on a timescale longer than $1/\delta\omega$.²⁸⁴ The spectral repulsion of random lasing modes

accelerate spatial decoherence. An incoherent sum of emission from many lasing modes, each producing a distinctly speckled wavefront, leads to low spatial coherence.^{285–288} Since the number of random lasing modes and their spatial structures is dictated by the amount of scattering in the random medium as well as the dimension and shape of the excitation region, the spatial coherence of random lasers can be tuned by varying the density of scatterers or the pump beam profile.

C. Speckle-free imaging

A random laser with low spatial coherence can suppress speckle noise and improve the image quality, especially when imaging in a scattering environment.^{289–295} Figure 22 shows full-field imaging through a (static) scattering film of a US Air Force resolution test chart through a thin static scattering film (S) with two illumination sources. Under spatially coherent illumination with a He:Ne laser, interference among scattered photons creates strong speckle noise that corrupts the image beyond recognition. In contrast, when illuminating with a random laser of low spatial coherence, scattered photons do not interfere, instead producing a uniform background. Although the photons that are scattered and mismatched to what would otherwise be dark regions of an image raise the background level and lower the image contrast, the features of the object remain clearly visible.

The speckle noise depends not only on the coherence properties of the illumination source, but also on the imaging optics, including the ratio of the numerical aperture for observation to that for illumination.²⁸⁹ Therefore, the degree of spatial incoherence in illumination that is needed to suppress speckle noise depends on the parameters of

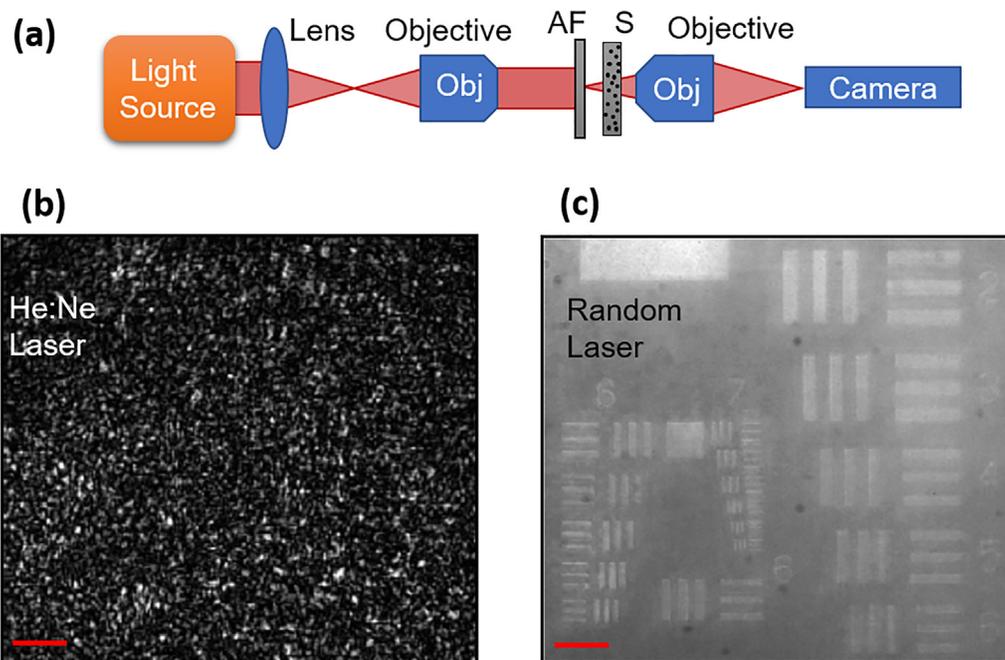


FIG. 22. Speckle-free imaging under random laser illumination. Reprinted with permission from Redding *et al.*, *Nat. Photonics* **6**, 355 (2012). Copyright 2012 Nature Publishing Group. (a) Schematic of full-field imaging of a US Air Force resolution test chart (AF) through a thin static scattering film (S). (b) Image is corrupted by speckle noise when the object is illuminated by a coherent He:Ne laser ($\lambda = 633$ nm). (c) Image is free of speckle noise when the illumination source is switched to a random laser with low spatial coherence.

a specific application, such as the amount of scattering or diffraction, the imaging resolution, etc. Correspondingly, a random laser can be tailored to provide sufficiently low spatial coherence for speckle suppression, while maintaining relatively high power per mode as compared to spatially incoherent sources such as lamps and LEDs. For example, to reduce the speckle contrast below the level observable by humans, it is sufficient to have 1000 spatial modes lase independently, which can be realized by engineering a random laser, but ordinary lamps and LEDs emit photons into far more modes, thus having lower power per mode.

A quantitative measure of the source brightness is the photon degeneracy parameter, which gives the number of photons per coherence volume.²⁶³ It is proportional to the spectral radiance, a radiometric measure of the amount of radiation through a unit area and into a unit solid angle within a unit frequency bandwidth. The photon degeneracy parameters for random lasers are several orders of magnitude higher than those of lamps and LEDs.²⁸⁹ The greatly improved brightness, together with short decoherence time, enables much higher speed for full-field imaging of transient physical processes. For example, a random laser is triggered to produce a short illumination flash at a well-defined time, providing uniform, speckle-free illumination for time-resolved microscopy.^{296,297}

D. Super-resolution spectroscopy

Super-resolution microscopy includes a set of imaging techniques that overcome the diffraction limit. One example is the single-molecule localization microscopy, which relies on spatially sparse activation of fluorescent molecules with a sample. Each molecule creates an isolated Gaussian-shaped disk in the image, and its center location can be fit with sub-pixel resolution. Although only a small number of molecules are recorded in one image, repetitive activation and recording under constant conditions allows full reconstruction of an object with a spatial resolution much finer than that of the imaging system.

The concept of super-resolution is extended to spectroscopy, using a random laser for sparse sampling in frequency.²⁹⁸ A 3D disordered sample with large gain volume has a huge number of spatial modes that may lase. If light scattering is relatively weak, these modes are spatially extended and overlap with each other. Their competition for optical gain will lead to spectral repulsion of the lasing modes.²⁹⁹ Since most of these modes have similar lasing thresholds, which ones will lase depends on initial seeding from spontaneous emission.³⁰⁰ When pumped by a short pulse, the initial photons spontaneously emitted into a subset of spatial modes will trigger the stimulated emission process, leading to a rapid growth of the number of photons in these modes. Hence, these modes tend to lase first; and once they lase, they will prevent other modes from lasing by saturating optical gain. For each pump pulse, only a small number of spatial modes manage to lase, correspondingly the emission spectrum contains a few narrow peaks. Due to spectral repulsion of the lasing modes, the emission peaks are well separated in frequency.³⁰¹ As the spontaneous emission events are stochastic and will seed different modes for individual pump pulse, the lasing modes vary from pulse to pulse, producing a distinct set of peaks in the emission spectrum. Because the spectral density of modes is uniform in a random medium, the lasing peaks collected over a large ensemble of pump pulses will cover the entire gain spectrum.

The sparse random lasing peaks in individual emission spectra provide spectral super-resolution when probing the frequency response of a sample. By recording the peak amplitudes and frequencies in incident and transmitted spectra taken with a series of random laser pulses, the transmission function of a sample is reconstructed.²⁹⁸ With only a few prominent peaks in each lasing spectrum, their center frequency is retrieved with high precision beyond the spectrometer resolution. Once a few thousands of lasing peaks are collected and analyzed, a plot of their amplitude change vs their center frequency gives the transmission function of the sample.

Figure 23 shows the transmission spectrum of a low-finesse Fabry-Pérot (FP) etalon, which is reconstructed with random lasing emission from a dye solution with ZnO nanoparticles.²⁹⁸ The dye molecules are optically pumped with frequency-doubled Nd:YAG laser pulses. The pump power and excitation volume are adjusted to keep the number of random lasing peaks in each shot low enough, so that the peaks are well separated in frequency. A threefold increase in spectral resolution is obtained. The ultimate resolution limit is set by the linewidth of individual lasing modes.

We note that amplified spontaneous emission (ASE) also creates sharp spikes in the emission spectrum, which originate from the spontaneously emitted photons taking long propagation paths inside a random medium and pick up a large amplification. These spikes are intrinsically stochastic and vary from shot to shot. Since different ASE spikes originate from independent spontaneous emission events, their frequencies are uncorrelated, and the Poisson statistics of the frequency spacing of neighboring ASE spikes results in a high probability of spectral bunching of ASE spikes in a single shot.³⁰² Once the pumping level is above the random lasing threshold, the lasing peaks have much higher amplitudes than the ASE spikes, and the inherent spectral separation of random lasing modes greatly reduces the probability of having two almost-degenerate peaks in the same shot spectrum. This is the key to sparse sampling in frequency.

While it is experimentally demonstrated in the visible frequency, the spectral super-resolution can be obtained in different frequencies ranging from ultraviolet to terahertz, where random laser sources are already available. Furthermore, this technique is robust and does not require any stabilization of the source, which is necessary in other high-resolution spectroscopy techniques such as frequency comb spectroscopy.

E. High power with high efficiency

There has been rapid progress in the development of random fiber lasers that generate high power with high efficiency and provide extremely broad wavelength tunability.³⁸⁰ While the fiber waveguide geometry provides transverse confinement for light, in the longitudinal direction the naturally present refractive index irregularities causes Rayleigh scattering, which is weak but sufficient for random lasing in a long fiber.²⁷² Much stronger feedback is supplied by artificial structures such as fiber Bragg gratings (FBGs) with random phase and/or amplitude modulation³⁰³ or an array of FBGs with randomly varying spacing,³⁰⁴ to realize lasing in short fibers.

In addition to stimulated emission, optical gain can be provided by stimulated Raman scattering (SRS) or stimulated Brillouin scattering (SBS) in a fiber.³⁰⁵ One unique property of SRS-based random distributed feedback fiber lasers is the ultra-wide wavelength tunability, as both stimulated Raman scattering gain and Rayleigh scattering

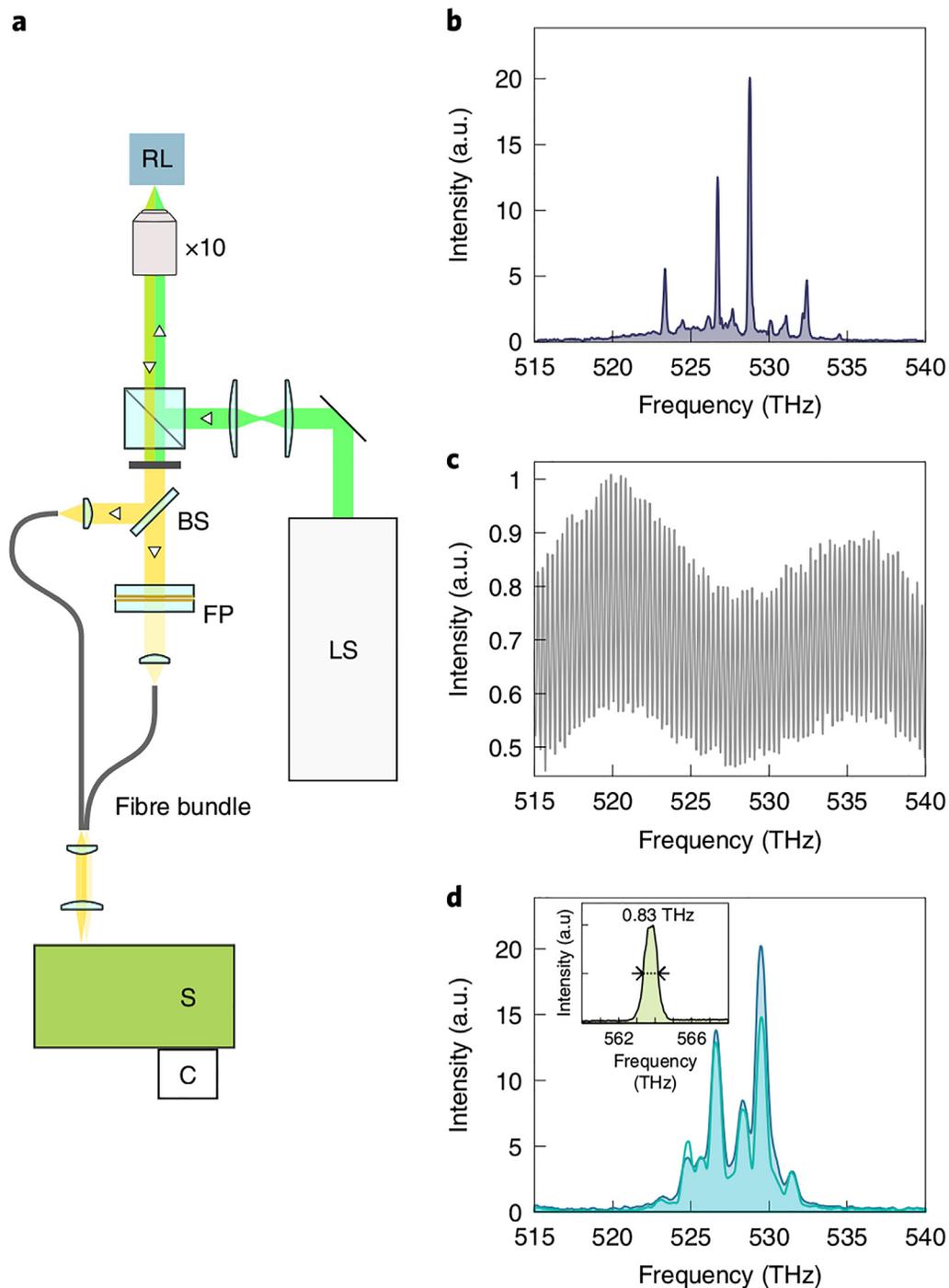


FIG. 23. Super-resolution spectroscopy using random laser emission. Reprinted with permission from Boschetti *et al.*, *Nat. Photonics* **14**, 177 (2020). Copyright 2020 Nature Publishing Group. (a) A random laser (RL) is optically pumped by a pulsed laser source (LS) with an objective lens ($\times 10$), and its emission in backward direction is collected by the same objective. A beam splitter (BS) sends a reference signal to a first multimode fiber, and the probe passes through an Fabry-Pérot (FP) etalon before being focused on a second fiber. The two fibers are bundled and simultaneously imaged onto the entrance slit of a spectrometer (S) so that they are spectrally dispersed and collected by a single camera (C) at the spectrometer output port. (b) A single-shot transmission spectrum of the FP etalon (cyan) is compared to its respective reference spectrum of random laser emission (light blue curve). Both are measured with a low-resolution spectrometer whose instrumental response is shown in the inset. (c) Transmission curve of the FP etalon, obtained by sparse sampling with a few thousands of random laser emission spectra, agrees to the one measured with a high-resolution spectrometer (not shown). (d) Transmission curve obtained with a broadband lamp illumination fails to capture the fine features in the transmission function of the FP etalon.

feedback are available at any wavelength.^{306–311} When pumped by a Yb-doped fiber laser or a narrow-band ASE source, cascaded Raman lasing up to the 10th order is obtained with increasing pump power.^{312–316} With wavelength tuning of the pump light, the Raman emission fills the spectral gaps between cascaded Stokes. As shown in Fig. 24, continuous wavelength tuning from 1 μm to 1.9 μm is demonstrated experimentally.³¹¹

Another striking feature of the SRS random fiber laser is high-efficiency high-power generation.³¹⁷ In order to concentrate all power in the first-order Raman Stokes, the fiber length is chosen to be relatively short to avoid power transfer to higher orders.^{318–324} One end of the fiber is terminated by a highly reflective FBG to ensure the total power output from the other end. With a 90-meter-long large-mode-area fiber, an output power of 919 W is obtained at $\lambda = 1150$ nm.³²⁴ The random distributed feedback from Rayleigh scattering leads to a specific power distribution along the fiber, making the generation efficiency superior to that of a conventional fiber laser with a Fabry–Pérot cavity.^{315,325,326} The maximum optical conversion efficiency has reached 89%, as a result of highly efficient Raman gain and low quantum defect. Another advantage is the absence of photo-darkening effect that happens to high-power fiber lasers based on stimulated emission.

High spectral purity and clean output beam profile are obtained with random distributed feedback lasers. The temporal stable emission is used to seed a kilowatt fiber amplifier.³²⁷ The absence of nonlinear

spectral broadening, which is common to traditional master-oscillator power-amplifiers, allows further power scaling and spectral beam combination for high-power narrow-linewidth applications. Thanks to its wavelength flexibility and low background noise, a random fiber laser is used to pump an optical parametric oscillator (OPO) to achieve tunable mid-infrared emission.³²⁸ Visible light is generated via second harmonics of a linearly polarized near-infrared random fiber laser emission with high conversion efficiency.³²⁹ Novel applications of random fiber lasers in telecommunication and remote sensing have been explored, see Refs. 330 and 331 and references therein.

F. Suppression of lasing instability

Instabilities and chaotic dynamics in the form of irregular pulsations are common to high power multimode lasers, hindering their applications in material processing, large-scale displays, laser surgery, and pumping other lasers. The spatiotemporal instabilities are intrinsic and caused by nonlinear light–matter interactions. For example, in a broad-area edge-emitting semiconductor laser, spatial hole burning and lensing effects results in formation of filaments, which are prone to modulational instabilities.³³² An efficient way of suppressing lasing instabilities while maintaining multimode operation is using a wave-chaotic cavity.³³³ In such a cavity, the interference of many propagating waves with random phases form speckles, which prevents self-focusing and filamentation, leading to stable lasing operation.

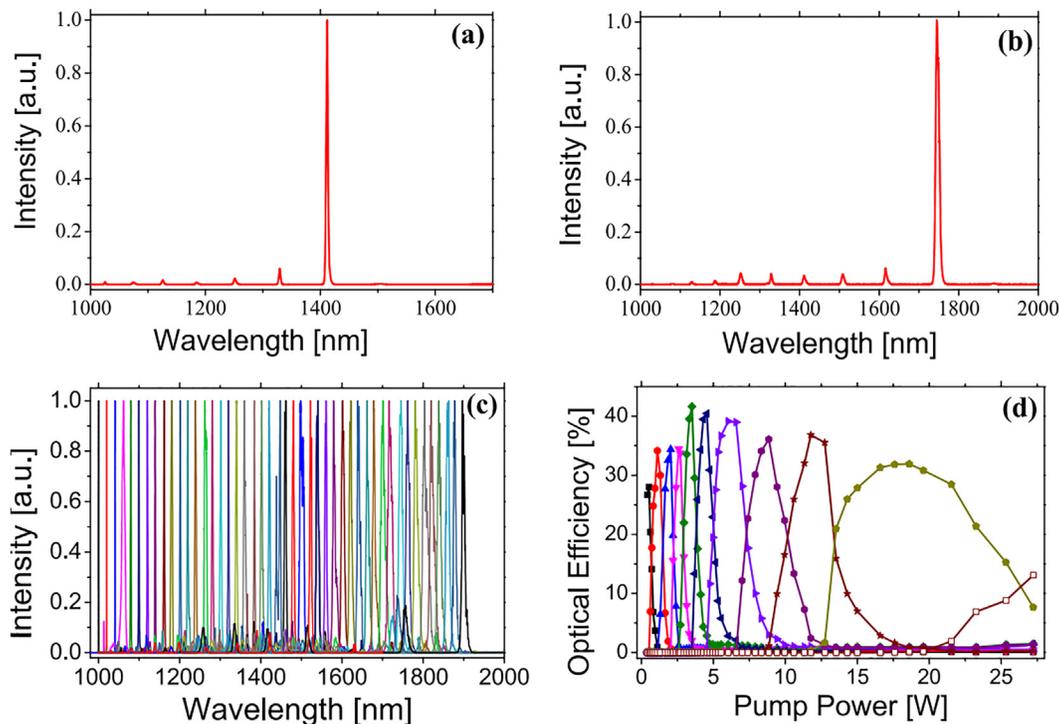


FIG. 24. Nearly octave wavelength tuning of a fiber random laser. Reproduced with permission from Zhang *et al.*, *Sci. Rep.* 7, 42611 (2017). Copyright 2017 Author(s); licensed under a Creative Commons Attribution (CC BY) license. A random distributed feedback fiber laser generates cascaded Raman Stokes up to the 10th order with increasing pump power. (a) and (b) are the output spectra of the laser when optimized for the 6th and 9th order Raman Stokes by tuning the pump power. The pump wavelength is 1025 nm. (c) shows the random fiber laser emission spectra with continuous wavelength tuning from 1 to 1.9 μm . (d) shows the optical efficiencies for different order Raman Stokes light as a function of the pump power.

Even in a narrow-stripe cavity that supports only one transverse mode, lasing dynamics is not always stable. In a Fabry–Pérot cavity formed by reflection from two end facets, lasing occurs in many longitudinal modes with equal frequency spacing. Optical interference between two modes creates periodic intensity modulation, and a refractive index grating is formed via optical nonlinearity. A third mode then diffracts from this grating, resulting in energy transfer among the lasing modes. The mode hopping and switching become more frequent and irregular in time at high pump power.³³⁴

To suppress lasing instability, random variation of the refractive index is introduced to an 1D dielectric stripe, as shown in Fig. 25(a). Multiple reflected waves interfere to form lasing modes with irregular frequency spacing.³³³ The mode structures also become irregular with varying spatial scales. Such irregularities disrupt coherent nonlinear interactions among the modes via multi-wave mixing, effectively blocking mode coupling and energy transfer. Numerical simulations reveal stable lasing dynamics over a wide range of pump power, in contrast to the cavity without refractive index fluctuation [Figs. 25(b) and 25(c)]. This simple approach is robust and generally applicable to other types of high-power lasers exhibiting instabilities.

IX. SUMMARY AND PERSPECTIVES

There are many ways to harvest disorder for photonic device applications, and it is impossible to cover all of them in this review. For example, randomly textured surfaces in solar cells have enhanced the efficiency of trapping and absorption of broadband light over a

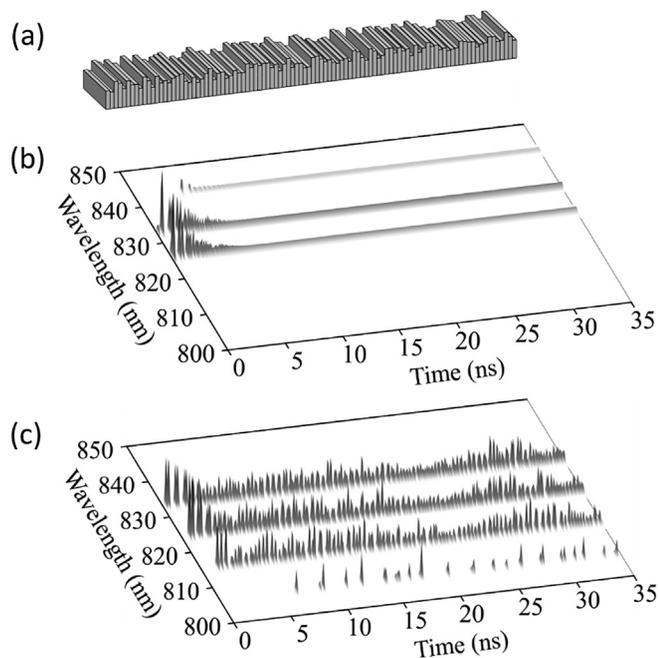


FIG. 25. Suppressing laser instability with structural disorder. (a) Schematic of introducing random variation of refractive index to an one-dimensional (1D) laser cavity. (b) Temporal evolutions of three longitudinal lasing modes reveal that they all reach a steady state after transient oscillations. (c) In a homogeneous cavity without refractive index fluctuation, all lasing modes pulsate irregularly and do not stabilize eventually.

wide angle of incidence.^{335–337} In nature, structural disorder has been maximized in white beetles scales to acquire an exceptional white appearance.^{35,338,339}

Various device applications rely on optical speckle patterns created by random scattering samples and multimode fibers/waveguides. A speckle pattern is sensitive not only to the incident wave but also to the internal structure of a sample and its environment. On one hand, if the sample and its environment remain constant, spatial, spectral, temporal, and polarization information of the illuminating light can be retrieved from the speckle pattern, as described in Secs. III–VII. On the other hand, by fixing the probe light and illumination condition, the speckle pattern may be used to sense the change of a sample or its surrounding. Section IX A will explain how disorder can enhance the sensitivity of optical sensors.

Looking ahead, there are a lot more opportunities to explore disorder for photonic device applications. When light propagates through a static disordered system, the information about incident light field is mixed but not lost. Such mixing of information can be used as a resource for computation, for example, high-dimensional matrix multiplication. In some sense, a strongly scattering medium is an optical realization of a neural network: the connection weights correspond to the coefficients of the field transmission matrix, and the nonlinearity comes from either nonlinear optical response of the material or simply the conversion of light field to intensity during detection by the camera. Section IX B will describe emerging applications of complex random systems for optical computing. Finally, we will briefly discuss the engineering of disorder for photonic device applications in Sec. IX C.

A. Disorder-enhanced optical sensors

A ground glass optical diffuser has been used to sense the refractive index change of surrounding liquid.³⁴⁰ When a laser beam of fixed wavelength passes through a solution and illuminates the diffuser, the speckle pattern it generates depends on the refractive index of the solution. A refractive index change as small as 0.00038 is detected with an average error less than 4.5%. Using more diffusers further enhances the sensitivity by multiple scattering of light.⁶² With three diffusers immersed in a solution, the solution's refractive index change is detected at resolution of 3.87×10^{-6} RIU, which is equivalent to the glucose concentration change of 12 ppm.

Another example is a pressure sensor. Remote sensing of pressure inside deformable microchannels has been realized with light scattering in a translucent Scotch tape.³⁴¹ As shown in Fig. 26, a change in the internal pressure of a deformable microchannel distorts the wavefront of a passing laser beam, which is subsequently incident on the Scotch tape and generates speckles in the far field. By detecting the change of speckle pattern, internal pressure can be remotely sensed with the resolution of 0.1 kPa within a pressure range of 0–3 kPa.

Optical speckles generated by multimode fibers have also been used for a variety of environmental sensing applications. In these applications, a laser beam with a constant wavelength is launched into a multimode fiber, and the transmitted/reflected speckles are monitored in time to track changes in the surrounding environment such as temperature,³⁴² pressure,³⁴³ acoustic vibrations,³⁴⁴ or properties of a liquid the fiber is immersed in.³⁴⁵ The speckle patterns can also detect tiny displacements or vibrations of the fiber position.^{346–348}

In addition to passive optical sensors, random lasers have been explored as active sensors with enhanced sensitivity.³⁴⁹ Since random

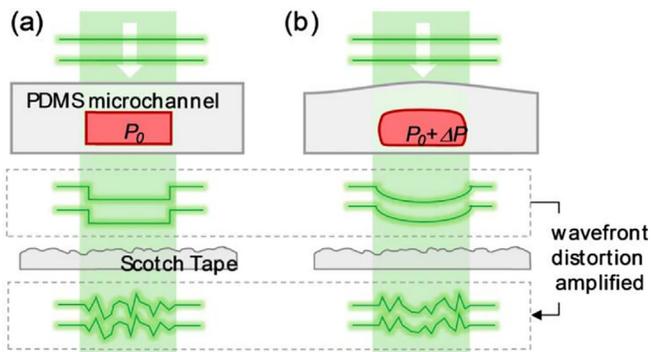


FIG. 26. Pressure sensing with laser speckle. Reprinted with permission from Kim *et al.*, *Opt. Lett.* **41**, 1837 (2016). Copyright 2016 The Optical Society. (a) Schematic diagram describing the change in wavefront of a laser beam, which passes through a transparent channel and a scattering layer (Scotch tape). (b) Deformation of wavefront caused by increase in internal pressure, and the scattering layer amplifies the wavefront change.

lasing action strongly depends on the amount of optical scattering, its emission is used to map cancerous tissue *ex vivo*.³⁵⁰ A human tissue is infiltrated with a dye solution and optically pumped by a laser. As the strength of light scattering in malignant tissue differs from that of the healthy one, the random lasing emission spectrum is modified. To avoid injection of toxic substance to biological tissue, the laser dye solution is contained in a transparent cell and separated from the scattering tissue.³⁵¹ Such design facilitates the application of random laser sensors to *in-vivo* measurements. Alternatively, biocompatible random lasers are made entirely of doped silk, functional in aqueous media.³⁵² They are capable of probing small changes in a chemical environment due to their intrinsic nonlinear response and spectral purity.

B. Disorder-assisted optical computing

This subsection will illustrate how disorder can assist optical computing with three examples.

1. Random projection

Random projections have been widely used in signal processing and machine learning applications. They require either to store a very large random matrix, or to use a different, structured matrix to reduce the computational and memory costs. This difficulty is recently overcome by using multiple scattering media to perform random projections without having to store any matrix in memory.³⁵³ Experimentally, a monochromatic laser illuminates a digital micromirror device (DMD), which spatially encodes digital information on the light beam by amplitude modulation. The light beam carrying the signal transmits through a layer of titanium dioxide nanoparticles, and the far-field speckle pattern is recorded by a camera. For a stable medium, such as a paint layer on a glass slide, the transmission matrix that maps incident fields to transmitted fields is stable, and thus, the scattering medium can therefore provide a convenient platform for random projections, without the need to determine the field transmission matrix. The resulting random projection of digital data is used for classification, and its efficiency is comparable to that of synthetic random projection.³⁵³ The large dimensional (10^4 – 10^6) random

projections are obtained almost instantaneously with disordered samples, which can be used for machine learning applications such as kernel classification.

2. Reservoir computing

Reservoir computing is a recent computational paradigm based on recurrent neural network. It expands the dimensionality of a problem by mapping an input signal to a higher-dimensional reservoir space, in order to capture and predict complex, non-linear temporal dynamics. Large reservoirs are difficult to obtain in conventional computers, due to extraordinary computation complexity and memory usage. There have been much interest and development of optical reservoir computing.^{354,355} One scheme utilizes multiple scattering of light in a disordered system.³⁵⁶

In reservoir computing, the most computationally demanding operation is the iterative computation of the reservoir state, which can be accelerated optically with a random scattering medium.³⁵⁶ The strong optical scattering guarantees random coupling weights of a very large number of photonic nodes and their parallel processing. Even though other steps related to the final linear layer are still performed on a conventional computer, the optical reservoir computing strategy is shown to outperform electronic implementations by two orders of magnitude in speed, and scale to very large dimensions, which cannot be reached in electronics due to memory limitations (Fig. 27). The scalability is demonstrated by predicting multidimensional large chaotic systems using optical reservoirs with up to 50 000 optical nodes.³⁵⁷

Multimode fibers/waveguides are also exploited for speckle-based optical reservoir computing.³⁵⁸ An electro-optical reservoir computer uses speckles generated by propagating a laser beam modulated with a SLM through a multimode waveguide to perform a multivariate audio classification task. Since the feedback and nonlinearity are provided by the SLM and a computer, one optical-to-electrical-to-optical conversion has to be done per pixel per time step. Moreover, such implementation requires as many SLM pixels as the number of neurons. In a latest proposal, the electrical feedback is replaced by optical feedback in a multimode waveguide ring resonator with a built-in nonlinear element.³⁵⁹ Elimination of the analog-digital conversion and the SLM paves the way toward fast, efficient reservoir computers for optical signal processing.

Expanding from spatial domain, multidimensional speckle dynamics in multimode fibers has been utilized for information processing.³⁶⁰ The input information is mapped into the space, frequency, and time domains by an optical phase modulation technique. The speckle-based mapping of input information is high dimensional and nonlinear, and thus, nonlinear time-dependent information processing can be achieved at fast rates. Using a reservoir computing approach, chaotic time-series prediction is realized at input rates of 12.5 Gigasamples per second. The passivity of multimode fibers allows multiple tasks to be simultaneously processed, which will further increase the processing speed.

3. Reconfigurable operations

Complex optical systems driven by wavefront shaping can perform various operations on classical and quantum light. They are programmable and reconfigurable, leading to promising applications for large-scale classical and quantum circuits.^{361–364} From a large field transmission matrix of a complex system, small matrices for desired linear operations have been extracted by finding suitable input and

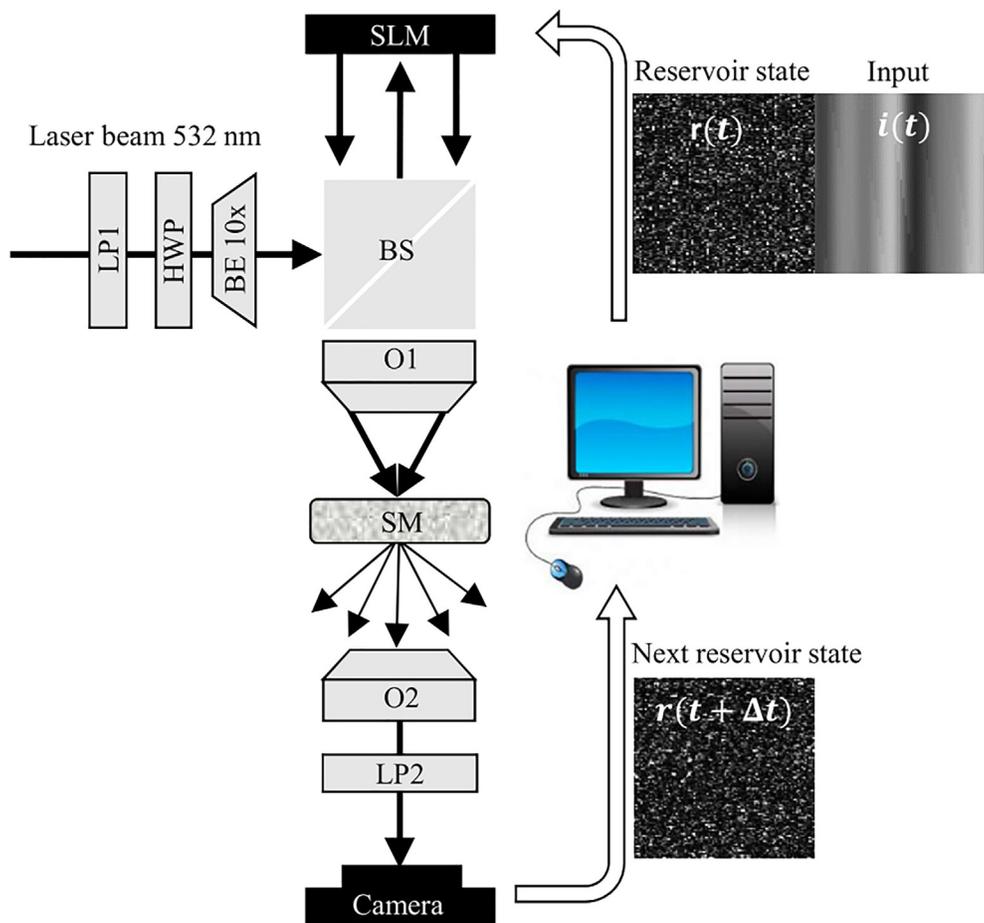


FIG. 27. Optical reservoir computing with random scattering medium. Rafayelyan *et al.* Phys. Rev. X **10**, 041037 (2020). Copyright 2020 Author(s); licensed under a Creative Commons Attribution (CC BY) license. The SLM receives from the computer the consequent input concatenated with the reservoir state and imprints it into the spatial phase profile of the reflected beam (upper inset). The scattering medium (SM) provides a complex linear mixing of the whole encoded information. Finally, the camera performs a non-linear readout for the next reservoir state (lower inset), which is sent by the computer back to the SLM to be displayed with new input, and the process repeats.

output projectors.³⁶³ The input projection is carried out by a SLM, which is placed next to a multimode fiber. By displaying a specific pattern on the SLM, the fiber acts as a desired complex-valued linear operator on the optical field. Using different input projections by the SLM, multiple linear operators are constructed with the same fiber. This work offers the prospect of reconfigurable linear optical analog computation units. Extending from classical to quantum regime, the reliable reprogrammable linear transformations open the door to scalable, reconfigurable quantum circuits.³⁶⁴

Beyond the passive random systems, random lasers with extraordinary complexity and strong nonlinearity may be suitable for reservoir computing. The spatiotemporal interference of numerous lasing modes in disordered media can be a source of massive-parallel random number generation.³⁶⁵

C. Engineering disorder

Moving beyond harvesting disorder is engineering disorder for photonic devices.^{34,35} Instead of complete disorder,

incorporating short-range or long-range order to nanostructures may further enhance device performance. It has been shown that introducing spatial correlations to disordered structures improves photon management and efficiency of thin-film solar cells.^{366–369} Specially designed disordered structures^{199,370} and metasurface diffusers³⁷¹ not only minimize energy loss and eliminate laborious calibration procedures, but also provide large noise tolerance, reliable reproducibility, and robustness against misalignment. In nature, amorphous photonic structures with short-range order³⁷² are widely adopted to produce angle-invariant color,^{373,374} in contrast to iridescent color created by ordered structures. Bioinspired photonic structures with correlated disorder³⁶ or hyperuniformity³⁴ are fabricated and explored for various applications, for example, special coloration effects^{35,375,376} and thin photovoltaic absorbers.³⁷⁷ Compared to random lasers, employing deterministic aperiodic nanostructures³⁷⁸ leads to control and reproducibility of lasing mode frequencies and spatial profiles.³⁷⁹ In between order and disorder, there is a huge parameter space to explore for photonic device applications.

NOMENCLATURE

Symbol

a_m	Modal complex amplitude	L	Linear dimension of a spectrometer system
$A(t)$	Time resolved amplitude	\mathcal{L}	Scattering path length distribution
$A(\omega)$	Spectral amplitude	L_{MMF}	Multi-mode fiber length
C_E	Spectral field correlation function	$\langle \mathcal{L} \rangle$	Average scattering path length
C_i	Cross-correlation coefficients of R_s with $i = \{x, y, xy, +\}$ polarized references	l_t	Scattering mean free path
C_I	Spectral intensity correlation function	l_s	Transport mean free path
C_S	Spectral correlation function	L_s	Scattering system thickness
C_t	Transmitted speckle intensity contrast	L_w	Fiber length
C_r	Speckle contrast	$\Delta \mathcal{L}$	Scattering path length distribution width
D_a	Input aperture diameter	m	magnification ratio
D_w	Fiber core diameter	\mathbf{M}_F	Random lens field transmission matrix
DOF	Depth of field	M_w	Number of guided modes
\mathbf{E}_{in}	Random lens input field	\mathbf{M}_{HH}	Horizontal to Horizontal polarization scattering matrix
\mathbf{E}_{in}^H	Horizontally polarized input field	\mathbf{M}_{HV}	Horizontal to Vertical polarization scattering matrix
\mathbf{E}_{in}^V	Vertically polarized input field	\mathbf{M}_{VH}	Vertical to Horizontal polarization scattering matrix
E_{MMF}	Multi-mode fiber output field	\mathbf{M}_{VV}	Vertical to Vertical polarization scattering matrix
\mathbf{E}_{out}	Random lens output field	N_λ	Number of distinct incoherent speckle patterns
\mathbf{E}_{out}^H	Horizontally polarized output field	NA	Numerical aperture
\mathbf{E}_{out}^V	Vertically polarized output field	N_i	Number of input channels
E_p	Speckle field pattern	N_{in}	Number of input polarization states
$E_s(\mathbf{r}, t)$	Spatiotemporal speckle field	N_o	Number of output channels
$E_t(\mathbf{r}, t)$	Transmitted spatiotemporal electric field	N_{out}	Number of input polarization states
$E(t)$	Time resolved electric field	N_r	Number of uncorrelated speckle patterns
$E(\omega)$	Spectral field	$N_x, N_{x,y}$	Number of spatial independent channels
\mathcal{F}	Fourier transform	N_λ	Number of spectral channels
f	Lens focal point	O	Sum of point sources
FOV	Field of view	O_λ	Multi-spectral object
FSR	Free spectral range	P	Point spread function (PSF)
$f(t)$	Laser pulse field	P_H	TE polarization spectral PSF
$F(\omega)$	Laser pulse field spectrum	P_V	TM polarization spectral PSF
$g(t)$	Transmitted/reflected laser pulse	P_λ	Multi-spectral point spread function
$G(\omega)$	Transmitted/reflected pulse field spectrum	r	Spatial radial coordinate
I	Total intensity	R_s	Correlated speckle pattern
I_{det}	Detector measured intensity	R_x	Reference speckle pattern with x-axis linear polarization
I_{dif}	Sensor array spectral intensity distribution	R_{xy}	Reference speckle pattern with 45° linear polarization
\mathbf{I}_{in}	Input intensity	R_y	Reference speckle pattern with y-axis linear polarization
I_{MMF}	Multi-mode fiber output intensity	R_+	Reference speckle pattern with right-handed circular polarization
\mathbf{I}_{out}	Output intensity	RES	Lateral resolution
I_p	Integrated intensity of speckle and reflected/transmitted pulses interference	\mathbf{S}	Stokes vector
I_q	Extracted intensity term of speckle and reflected/transmitted pulses interference	\mathbf{S}_{in}	Input Stokes vector
I_{sig}	Input spectral signal	S_1, \dots, S_4	Stokes parameters
\bar{I}_s	Average speckle intensity	SNR	Signal-to-noise ratio
$I_{sig}^{(H)}$	Input spectra for TE polarization	$T(\mathbf{r}, \omega)$	Frequency resolved field transmission matrix
$I_{sig}^{(V)}$	Input spectra for TM polarization	Δt	Temporal range
I_{1p}	One photon absorption time integrated intensity pattern	δt	Temporal resolution
I_{2p}	Two-photon absorption time integrated intensity pattern	$\Theta(t)$	Time resolved phase
I_λ	Multi-spectral intensity	$\theta_{TM}(\mathbf{r}, \omega)$	Transmission matrix spectral phase
$I(\omega)$	Power spectrum	x	Cartesian spatial coordinate x
		y	Cartesian spatial coordinate y
		z	Point source axial coordinate
		z'	Sensor axial coordinate
		z_{det}	Axial lens to detector distance
		z_{obj}	Axial object to lens distance
		z_{ref}	Axial reference source to lens distance
		β_m	Modal propagation constant

$\dot{\beta}_m$	Time derivative of modal propagation constant
$\Delta\theta_m$	Angular range of the memory effect
$\Delta\lambda$	Wavelength spacing
δ	Dirac delta distribution
$\delta\lambda$	Spectral resolution
$\delta\omega$	lasing modes frequency spacing
$\Theta(t)$	Time resolved phase
θ_{max}	Maximum angular range of light
θ_s	Scattering angle
θ_T	original input angle of light
$\theta(\omega)$	Spectral phase
$\theta_{TM}(\mathbf{r}, \omega)$	Transmission matrix spectral phase
λ	Wavelength
ρ	Point source radial coordinate
ρ_0	Reference point source transverse coordinate
ρ'	Sensor radial coordinate
σ_I	Speckle intensity standard deviation
ϕ	Azimuthal coordinate
Ψ	Mode spatial field profile
ω	Angular frequency
*	Convolution operation
*	Correlation operation
⊗	Deconvolution operator

Unit Description

as	attoseconds
cm	centimeters
dBm	decibel-milliwatts
fs	femtoseconds
GHz	Gigahertz
GSps	Giga samples per second
Hz	Hertz (s^{-1})
kPa	Kilopascal
m	meters
MHz	Megahertz
mm	millimeters
MSps	Mega samples per second
nm	nanometers
ns	nanoseconds
pm	pedometers
ppm	Parts per million
ps	picoseconds
RIU	Refractive index unit
THz	Terahertz
°	Angular degree
μm	micrometers

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AUTHOR DECLARATIONS

Conflict of Interest

The authors have no conflict of interest to declare.

DATA AVAILABILITY

Data sharing is not applicable to this article as no new data were created or analyzed in this study.

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